

# Calphad modeling of liquid phase models & ML support

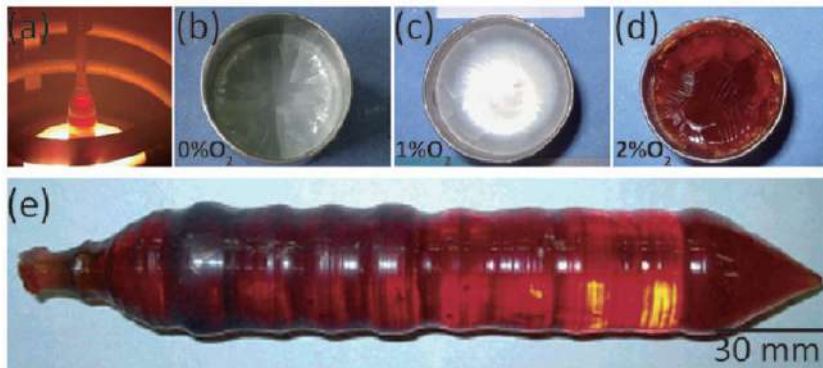
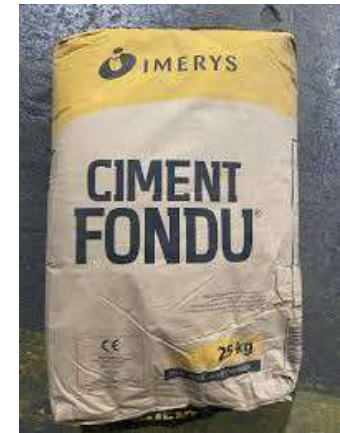
A. Pisch, G. Deffrennes, P. Benigni, C. Gueneau



Journées Liquide – 29 Novembre 2024 – Paris



# Motivation



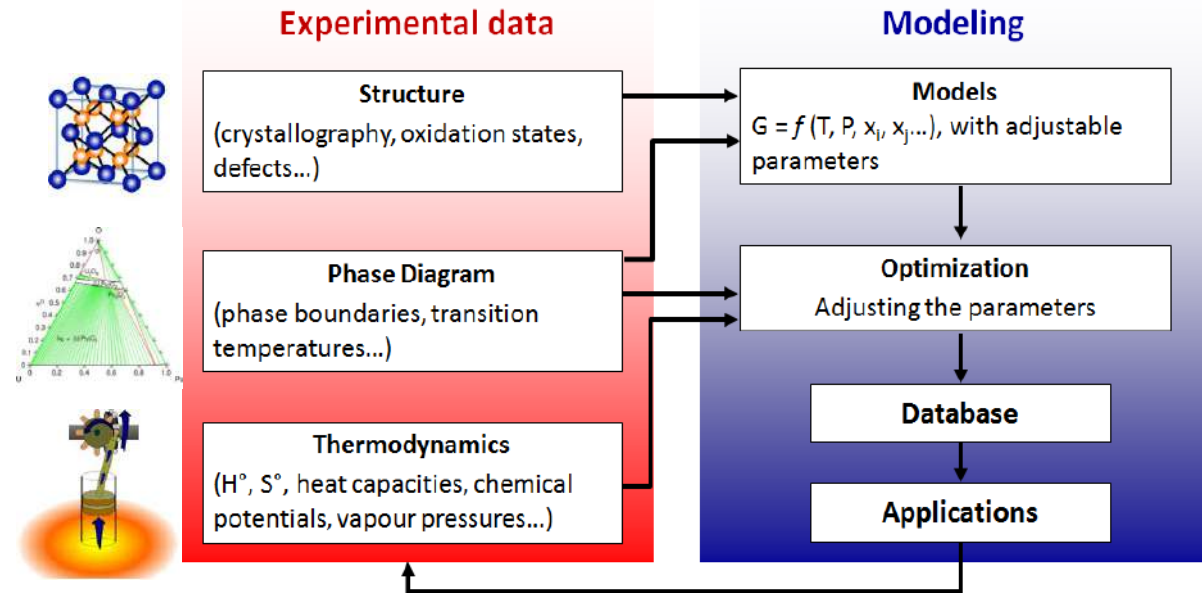
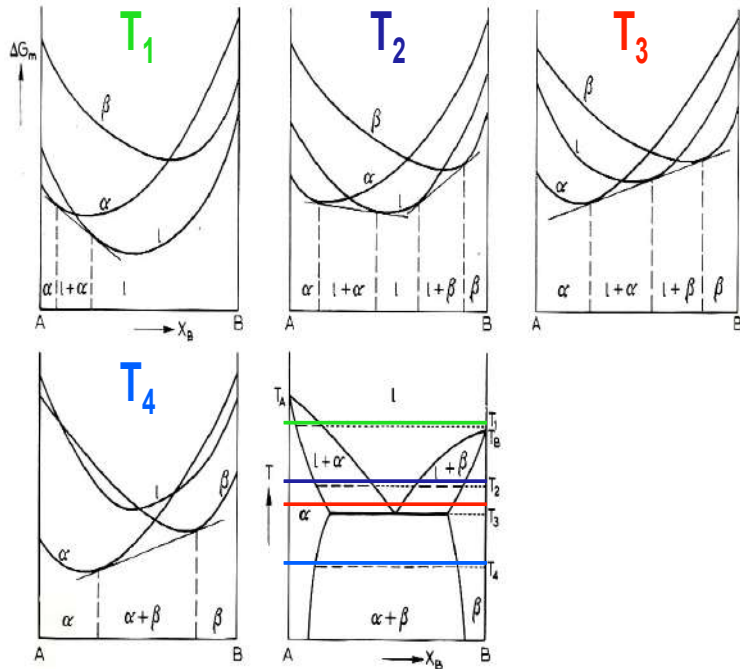
# Outline

- The Calphad methodology
- Thermodynamic modeling of liquids
  - First generation - Kaufmann & Bernstein (1970)
  - Second generation - A. Dinsdale (1991)
  - Challenges
- Third generation modeling : adding more physics
  - Einstein model for heat capacity  $C_p$
  - Two-state model for the liquid phase
- Modeling chemical interaction in the liquid phase
  - (Sub) regular solutions
  - Short range order – the ionic liquid model
- Machine learning on chemical interaction in the liquid
- Conclusions & Outlook

# Modélisation thermodynamique : Méthode CALPHAD



⇒ Couplage entre énergies de Gibbs et diagramme de phase



Les fonctions d'énergie de Gibbs des phases sont ajustées par une méthode aux moindres carrés pour reproduire les données exp. (thermodynamiques et de diagramme de phase)

→ 
$$\min(G) = \min\left(\sum_{\alpha} m^{\alpha} G_m^{\alpha}(T, p, x_i^{\alpha} \text{ or } y_k^{(l,\alpha)})\right)$$

$$x_i = \sum_{\alpha} m^{\alpha} \cdot x_i^{\alpha}$$

# The Calphad method

## Calphad allows to

- calculate stable and metastable equilibria in multicomponent systems
- evaluate the coherence of experimental & theoretical data
- Extrapolate to unknown areas in the composition / temperature / pressure space
- link multicomponent thermodynamics to engineering codes : Aspen, ...
- Cover the full temperature range from 0K to (at least) 6000K

## Many databases are available

- general purpose databases : SGTE solution, SGTE substance, FTPs,
- databases by chemistry : alloys (ferrous, Al, Mg ...), oxides, salts,...
- databases by application : HEA, light metal, solders...
- aqueous solutions

## Calphad can not

- Predict unknown compounds & phases
- Give physical meaning to the model parameters



# Modeling of liquid phase -1<sup>st</sup> generation

L. Kaufman & Bernstein (1970) “Computer Calculation of Phase Diagrams”

- Focus on Refractory metals
- Relative Gibbs energies  
=> lattice stabilities

SUMMARY OF FREE ENERGY DIFFERENCES

Metal	Free energy difference (cal/g-atom)	Temperature (°K)
Zr	$\Delta F^{\beta \rightarrow L} = 4250 - 2.0T$	$\bar{T}^{\beta} = 2125$
	$\Delta F^{\epsilon \rightarrow L} = 5280 - 2.9T$	$\bar{T}^{\epsilon} = 1820$
	$\Delta F^{\alpha \rightarrow L} = 4480 - 2.9T$	$\bar{T}^{\alpha} = 1544$
	$\Delta F^{\beta \rightarrow \epsilon} = -1030 + 0.90T$	$T_0^{\beta \epsilon} = 1144$
	$\Delta F^{\alpha \rightarrow \epsilon} = -800$	
	$\Delta F^{\alpha \rightarrow \beta} = +230 - 0.90T$	$T_0^{\alpha \beta} = 255$
Hf	$\Delta F^{\beta \rightarrow L} = 4990 - 2.0T$	$\bar{T}^{\beta} = 2495$
	$\Delta F^{\epsilon \rightarrow L} = 6820 - 2.9T$	$\bar{T}^{\epsilon} = 2351$
	$\Delta F^{\alpha \rightarrow L} = 6020 - 2.9T$	$\bar{T}^{\alpha} = 2076$
	$\Delta F^{\beta \rightarrow \epsilon} = -1830 + 0.90T$	$T_0^{\beta \epsilon} = 2033$
	$\Delta F^{\alpha \rightarrow \epsilon} = -800$	
	$\Delta F^{\alpha \rightarrow \beta} = +1030 - 0.90T$	$T_0^{\alpha \beta} = 1144$



# Modeling of liquid phase -2<sup>nd</sup> generation

*CALPHAD* Vol. 15, No. 4, pp. 317-425, 1991  
Printed in the USA.

0364-5916/91 \$3.00 +.00  
1991 Pergamon Press plc

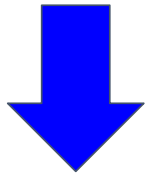
## SGTE DATA FOR PURE ELEMENTS

A T Dinsdale

Division of Materials Metrology, National Physical Laboratory,  
Teddington, Middlesex, TW11 0LW, UK

# Modeling of liquid phase -2<sup>nd</sup> generation

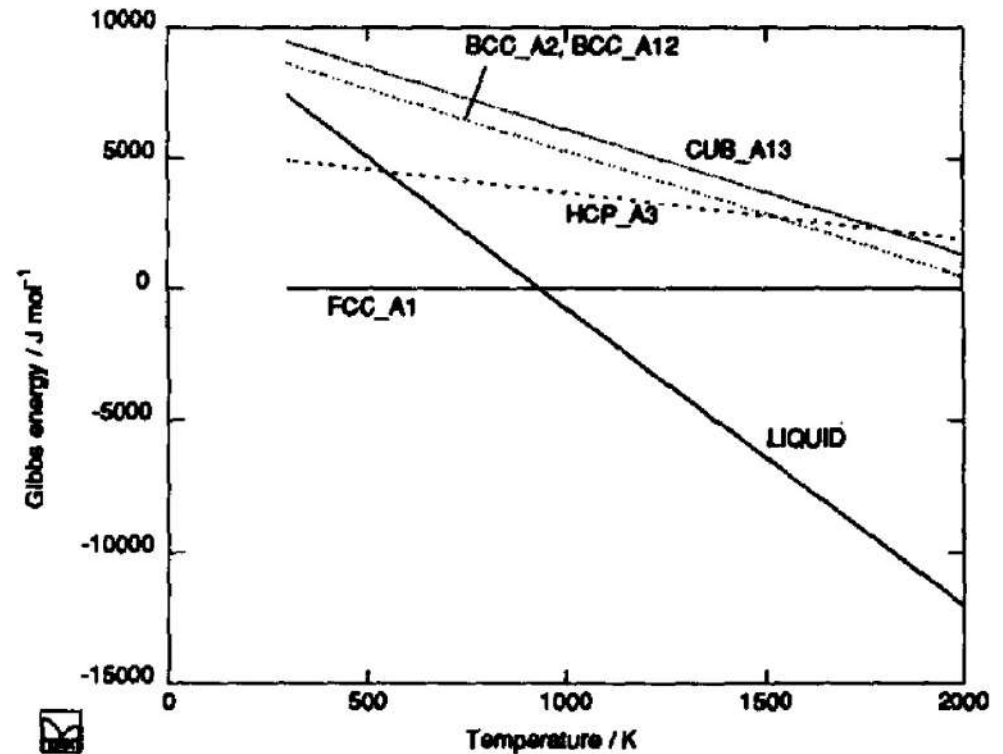
$$G = a + b T + c T \ln(T) + \sum d T^n$$



$$S = -b - c - c \ln(T) - \sum n d T^{n-1}$$

$$H = a - c T - \sum (n-1) d T^n$$

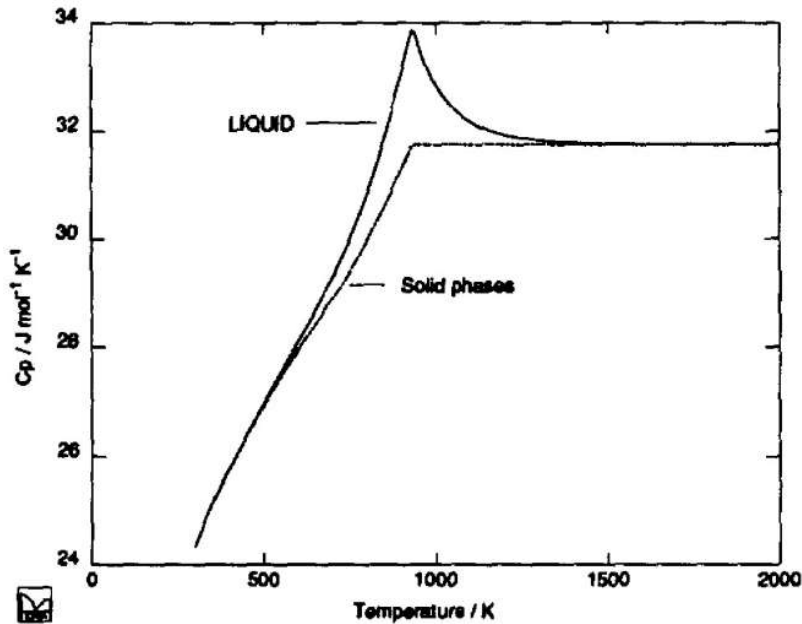
$$C_p = -c - \sum n (n-1) d T^{n-1}$$



Gibbs energy of phases of Al relative to FCC\_A1



# Modeling of liquid phase -2<sup>nd</sup> generation



Heat capacity of Al

FCC\_A1

$$\begin{aligned}
 & -7976.15 + 137.093038 T - 24.3671976 T \ln(T) - 1.884662E-3 T^2 - 0.877664E-6 T^3 + 74092 T^{-1} & (298.15 < T < 700) \\
 & -11276.24 + 223.048446 T - 38.5844296 T \ln(T) + 18.531982E-3 T^2 - 5.764227E-6 T^3 + 74092 T^{-1} & (700 < T < 933.47) \\
 & -11278.378 + 188.684153 T - 31.748192 T \ln(T) - 1.231E28 T^9 & (933.47 < T < 2900)
 \end{aligned}$$

LIQUID

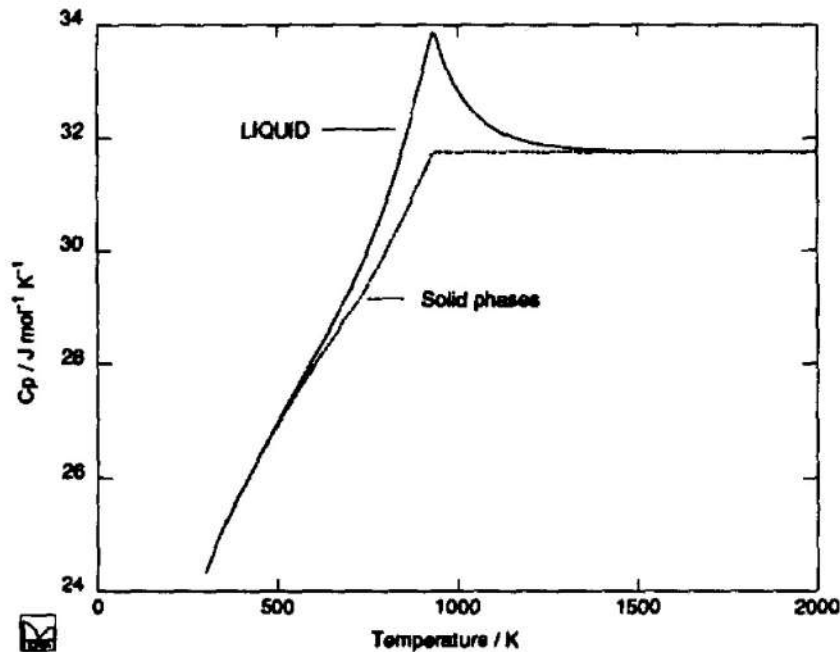
$$\begin{aligned}
 & 3028.879 + 125.251171 T - 24.3671976 T \ln(T) - 1.884662E-3 T^2 - 0.877664E-6 T^3 + 74092 T^{-1} + 7.934E-20 T^7 & (298.15 < T < 700) \\
 & -271.21 + 211.206579 T - 38.5844296 T \ln(T) + 18.531982E-3 T^2 - 5.764227E-6 T^3 + 74092 T^{-1} + 7.934E-20 T^7 & (700 < T < 933.47) \\
 & -795.996 + 177.430178 T - 31.748192 T \ln(T) & (933.47 < T < 2900)
 \end{aligned}$$

**LIQUID**

relative to FCC

$$\begin{aligned}
 & 11005.029 - 11.841867 T + 7.934E-20 T^7 \\
 & 10482.382 - 11.253974 T + 1.231E28 T^9
 \end{aligned}$$

# Modeling of the liquid phase - Challenges

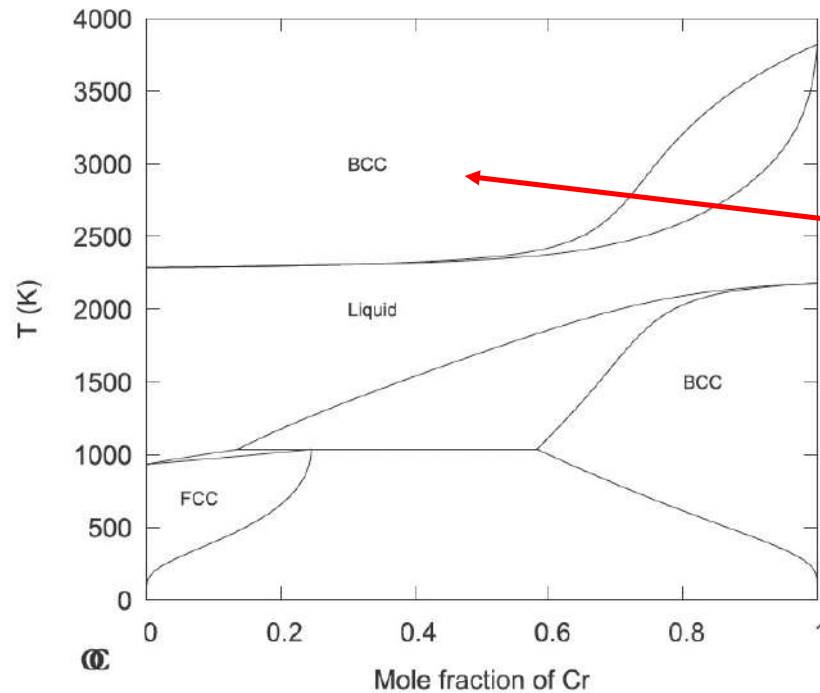


Heat capacity of Al

- Break points at melting are unphysical
  - 1st & 2nd derivative are not continuous
  - leads to unwanted kinks in  $C_p$  when combined in solid / liquid solutions
- Constant heat capacity for liquid is unphysical, especially at very high T (influence of density)

# Modeling of the liquid phase - Challenges

No breakpoint at melting point



Stabilization of solid phases at high temperature !

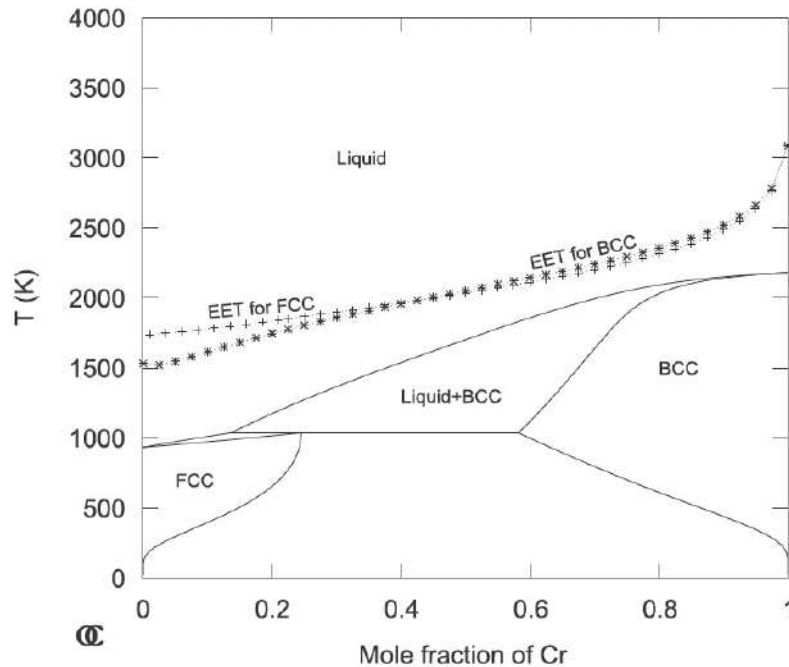
(a) Al-Cr no break points, no EEC

B. Sundman et al. Calphad 68 (2020): 101737

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# Thermodynamic modeling of the liquid phase - Challenges

## Solution I : Equal Entropy Criteria EEC



(b) Al-Cr no break points, with EEC

B. Sundman et al. Calphad 68 (2020): 101737

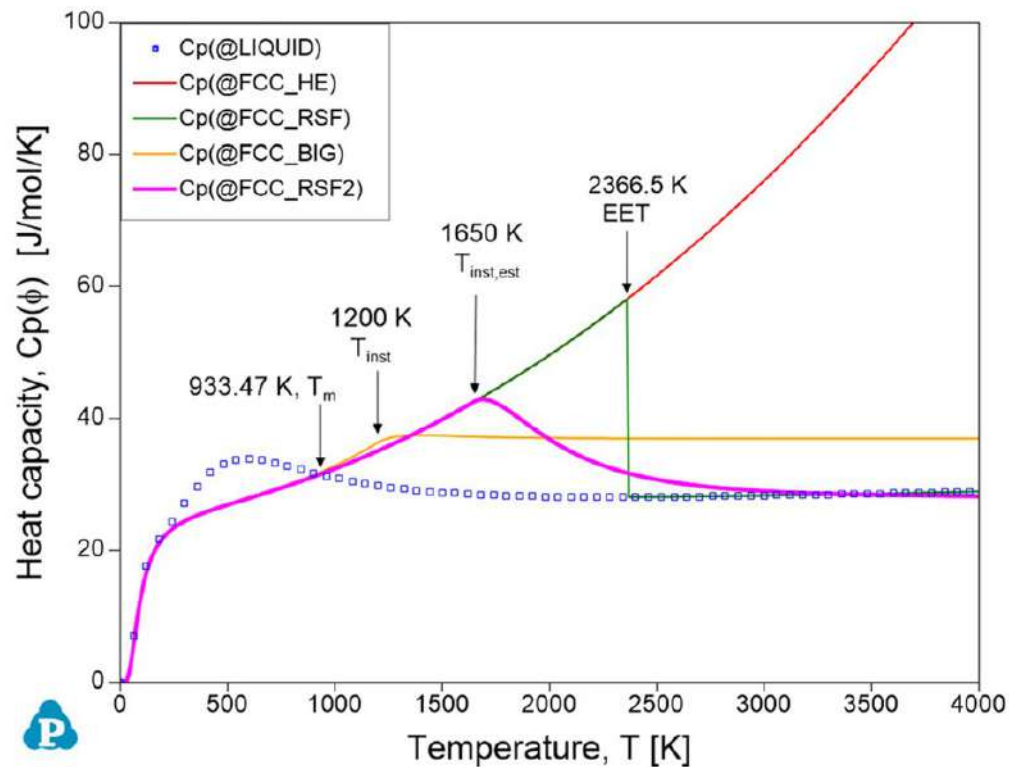
Gibbs energy minimizer software related

1. Gibbs energy & entropy are checked prior to equilibrium calculation in the full temperature range
2. If  $S(\text{solid}) > S(\text{liquid})$ , the solid phase is withdrawn from the equilibrium calculation

EEC is programmed in OpenCalphad & ThermoCalc

# Thermodynamic modeling of the liquid phase - Challenges

Solution II : Extend solid above  $T_f$  + change in slope



Slope change above fusion

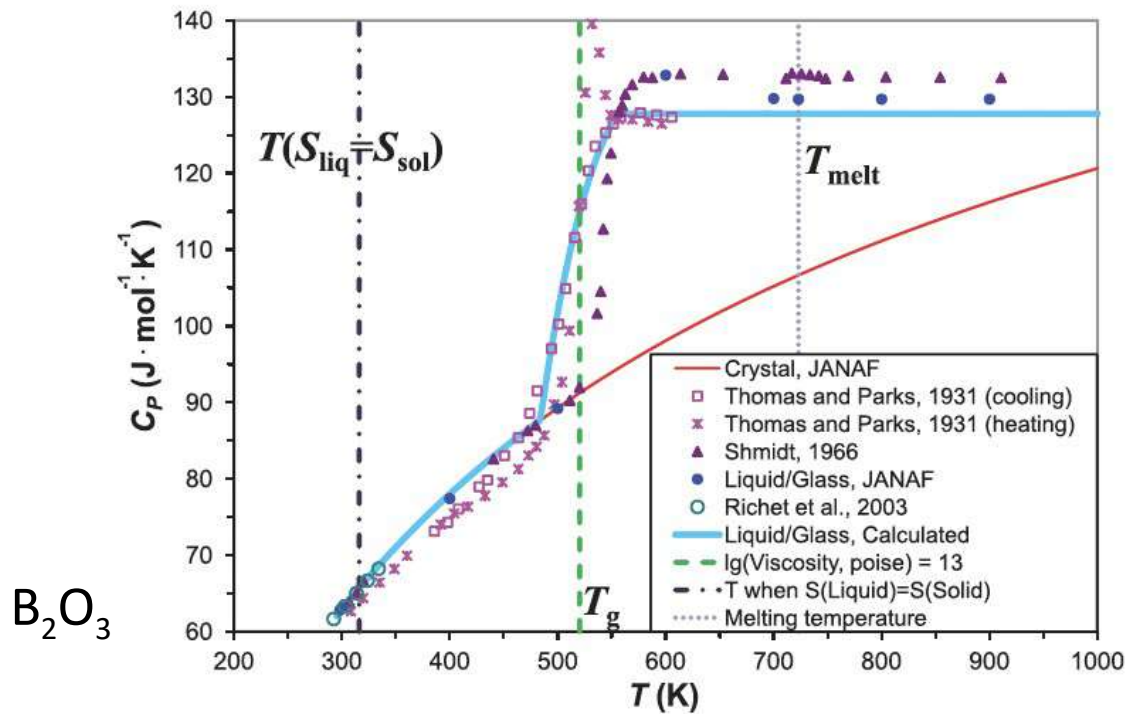
- better for solution phases : no/less kinks in  $C_p$  curves
- implemented in all softwares
- drawback of 1st and 2nd derivative of  $G$  (solid) remains

R. Schmid-Fetzer, JPED 43(3) (2022): 304-316.

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# Modeling of the liquid phase - Challenges

Extrapolation of liquid down to RT -> glass transition



## 2nd generation approach

- fitting the glass transition with three polynomial functions
- problem for 1st & 2nd derivative of the Gibbs energy
- problem on extrapolation in multicomponent systems

C.A. Becker et al. Physica Status Solidi (b) 251 (2014): 33–52

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# Modélisation CALPHAD 3<sup>ème</sup> génération des liquides unaires

P. Benigni



Journées des liquides hautes températures  
Paris, 29 novembre 2024



# Heat capacity of liquid metals

Stable liquid ( $T > T_m$ )

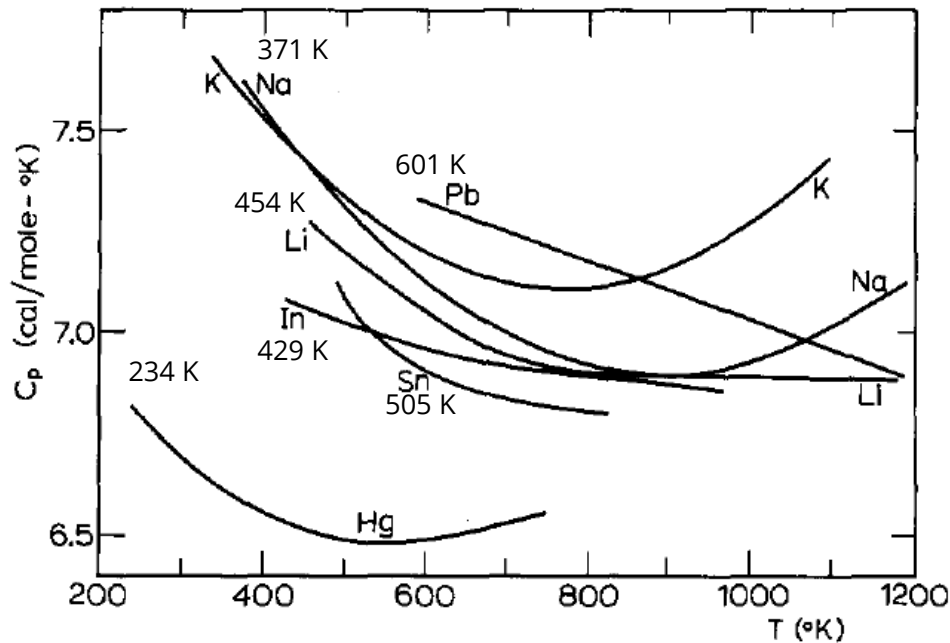


Fig. 1. Heat capacity at constant pressure of liquid metals

*T.W. Chapman, The heat capacity of liquid metals, Mater. Sci. Eng. 1 (1966) 65-69*

Stable ( $T > T_m$ ) and supercooled liquid ( $T < T_m$ )

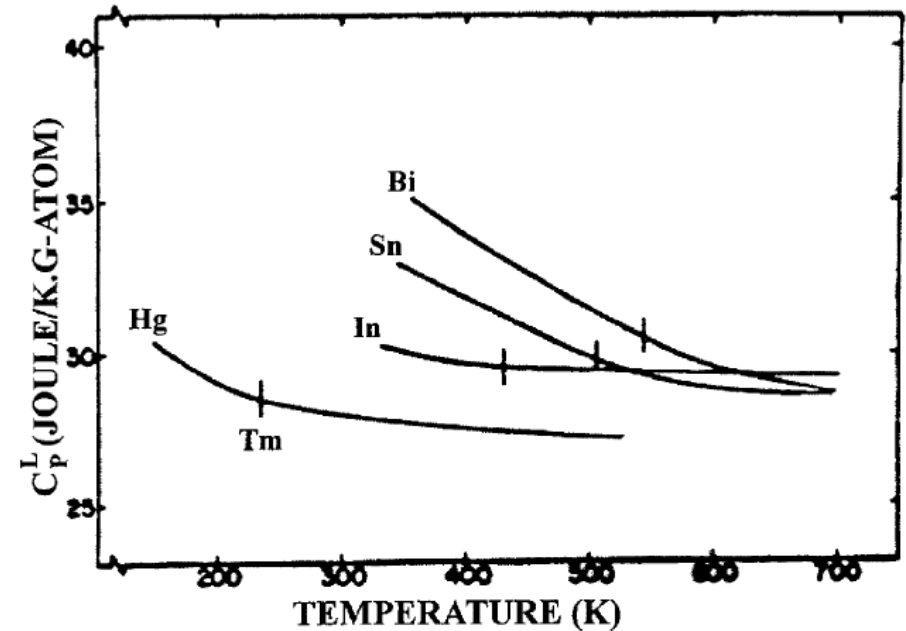
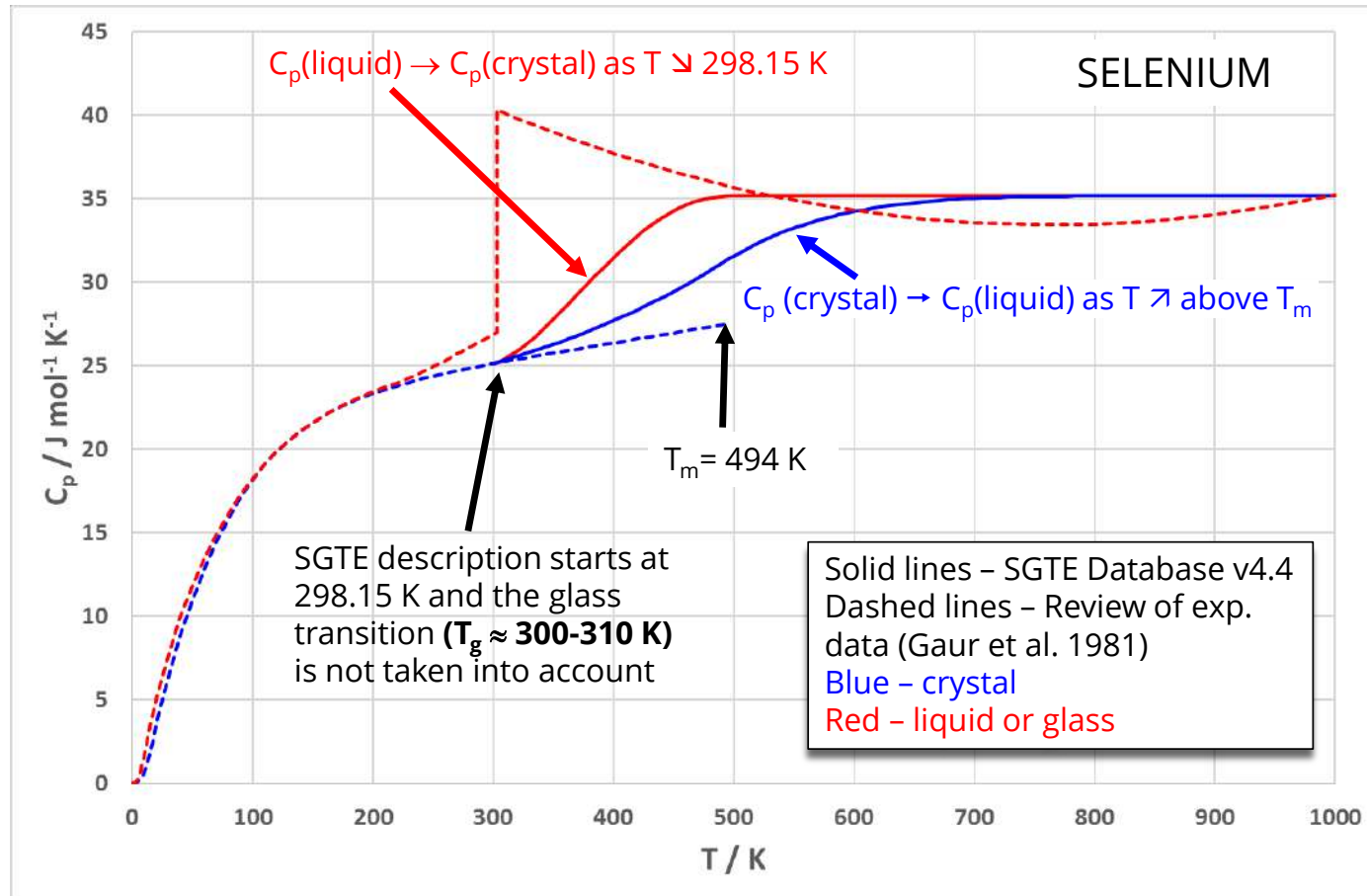


Fig. 3. Heat capacity of several liquid metals as a function of temperature. The vertical marks are the melting temperatures (after Perepezko and Paik [10]).

## Heat capacity of pure selenium, a glass forming element

- For each phase, including the liquid, various G analytical expressions are used over different T ranges, with several drawbacks



# The 2-state models, 100 years of history

- 2-level models have long been used in statistical physics
- In **crystals**
  - to describe **heat capacity anomalies** at low T (Schottky 1922) or explain some different kind of phase transitions (Strässler & Kittel 1965)
- The application to **liquids** consists in making the hypothesis that a pure substance at the liquid state is made up of 2 types of distinct structural entities
  - which may or may not form an ideal binary solution
- Within the CALPHAD community
  - In 1988, Agren proposed describing the liquid phase using an ideal 2-state model
  - **This choice is finally retained for the 3<sup>rd</sup> generation CALPHAD descriptions**
- In the glass community
  - 2-state models in various variants are used to describe the liquid phase by many authors: Macedo et al. (1966), Rapoport (1967), Angell & Rao (1972), Ponyatovsky et al. (1994), Moynihan (1997), Ojovan (2008), Holten et al. (2011)...



W. A. Schottky (1886-1976)

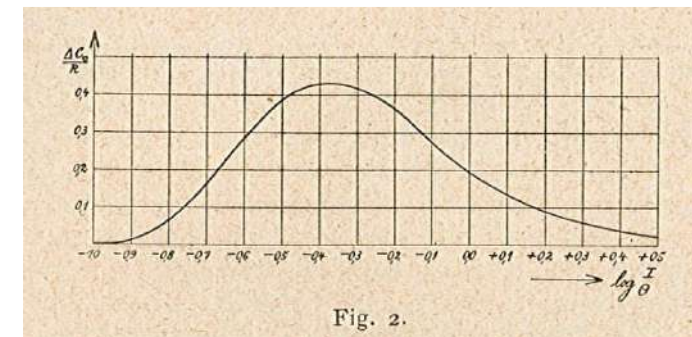


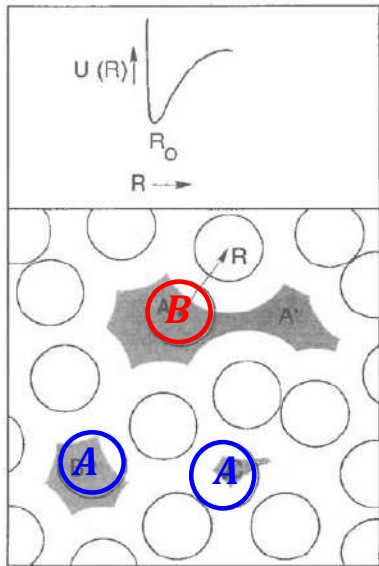
Fig. 2.

W. Schottky, Über die Drehung der Atomachsen in festen Körpern. (Mit magnetischen, thermischen und chemischen Beziehungen), *Phys. Zeitschrift*. 23 (1922) 448–455

# The ideal 2-state model

- Key assumption
  - liquid = ideal solution of 2 types of structural entities

(Fig. adapted from Debenedetti 1996 and Zallen 1983)



**B = liquid-like or gas-like** (translation + vibration) = excited state  
**A = solid-like** (vibration) = ground state

- that exchange through an equilibrium :  $A \rightleftharpoons B$

- The mole fractions  $\xi_A$  and  $\xi_B$  of  $A$  and  $B$  vary with the external variable  $T$
- Liquid Gibbs energy:  $G_L = \underbrace{\xi_A G_A^\circ + \xi_B G_B^\circ}_{\text{Mechanical mixture}} + \underbrace{RT(\xi_A \ln \xi_A + \xi_B \ln \xi_B)}_{\text{Ideal entropy of mixing}}$

- If  $\xi = \xi_B$  kept as the single **internal variable** = **non-conservative order parameter**

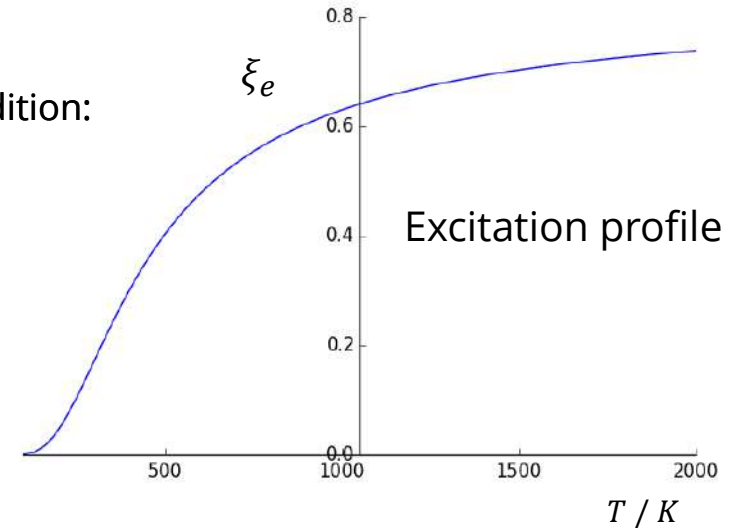
$$G_L = G_A^\circ + \xi \Delta G_d + RT((1 - \xi) \ln(1 - \xi) + \xi \ln \xi)$$

- With:  $\Delta G_d = G_B^\circ - G_A^\circ$

- The internal equilibrium condition:

$$\left( \frac{\partial G_L}{\partial \xi} \right)_{\xi = \xi_e} = 0$$

Gives:  $\xi_e = \frac{1}{1 + \exp\left(\frac{\Delta G_d}{RT}\right)}$



## Application to a real substance

- Liquid Gibbs energy :  $G_L = G_A^\circ - RT \ln(1 + \exp(-\Delta G_d/RT))$
- The 100% A phase = metastable liquid in internal equilibrium in which the structural entities only have vibrational degrees of freedom
  - Simple vibrational model based on a weighed sum of Einstein functions

$$C_p(T) = \sum_i 3R\alpha_i \left(\frac{\Theta_i}{T}\right)^2 \frac{e^{\Theta_i/T}}{(e^{\Theta_i/T} - 1)^2}$$

$$S(T) = \sum_i 3R\alpha_i \left(\frac{\Theta_i}{T} \frac{e^{\Theta_i/T}}{e^{\Theta_i/T} - 1} - \ln(e^{\Theta_i/T} - 1)\right)$$

$$H(T) - H(0) = \sum_i \alpha_i \frac{3R\Theta_i}{e^{\Theta_i/T} - 1}$$

- The Einstein temperatures  $\Theta_i$  and corresponding weights  $\alpha_i$  are adjustable parameters to be fitted to experimental results

- Gibbs energy difference between the two states
  - CALPHAD type expansion :  $\Delta G_d = A + BT + CT \ln T$
  - $A, B, C...$  coefficients to be fitted to experimental results

$$\Delta G_d = \Delta H_d - T\Delta S_d = A + BT + CT \ln T$$

$$\Delta S_d = -B - C(1 + \ln T)$$

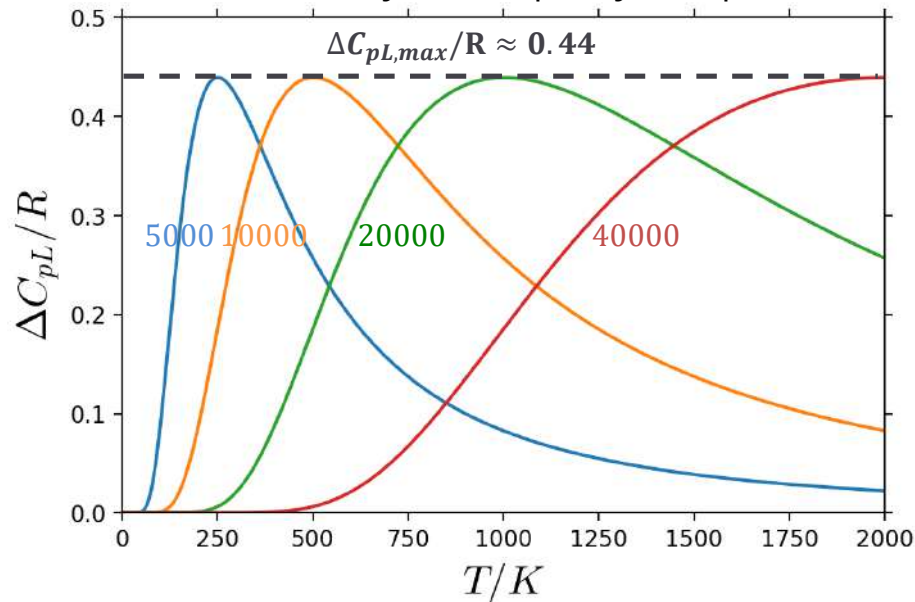
$$\Delta H_d = A - CT$$

$$\Delta C_{pd} = -C$$

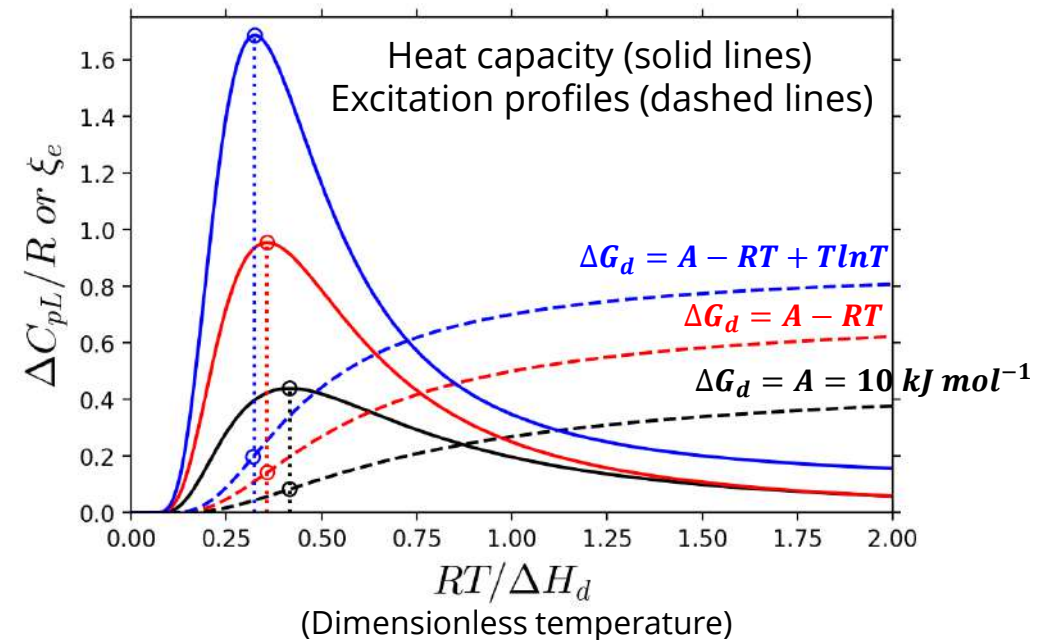
## Configurational part ( $\Delta$ ) of the thermodynamic functions of the liquid

- Gibbs energy:  $\Delta G_L = G_L - G_A^\circ = -RT \ln(1 + \exp(-\Delta G_d/RT))$ 
  - with:  $\Delta G_d = \Delta H_d - T\Delta S_d = \mathbf{A} + \mathbf{B}T + \mathbf{C}T \ln T$
- Heat capacity:  $\Delta C_{pL} = \left(\frac{\partial \Delta H_d}{\partial T}\right)_p \xi_e + \frac{\Delta H_d^2}{RT^2} \xi_e (1 - \xi_e)$

Effect of changing  $A$  ( $J \text{ mol}^{-1}$ ) with  $B = C = 0$   
Schottky heat capacity hump

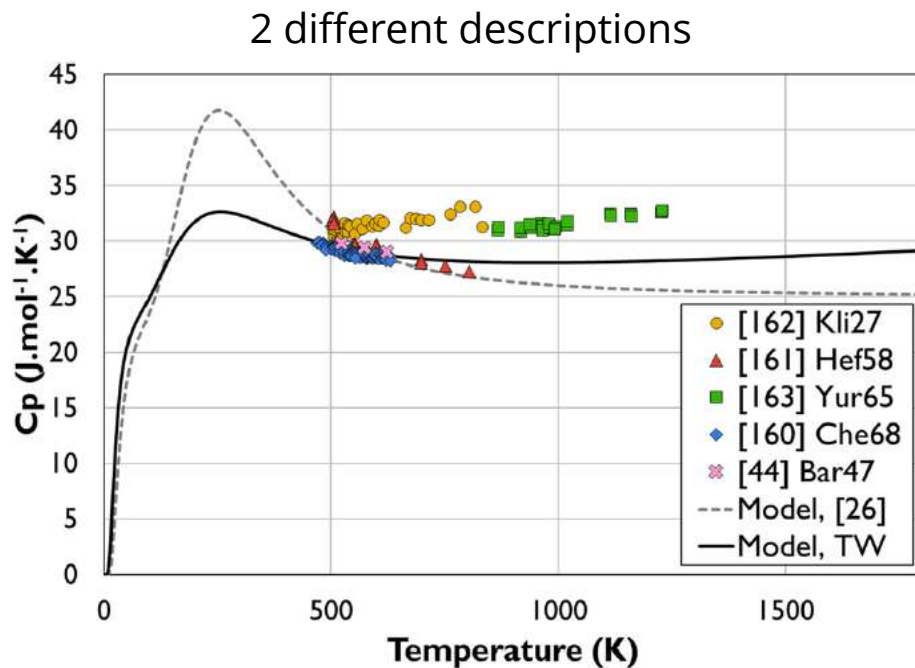


Effect of adding  $B$  and  $C$



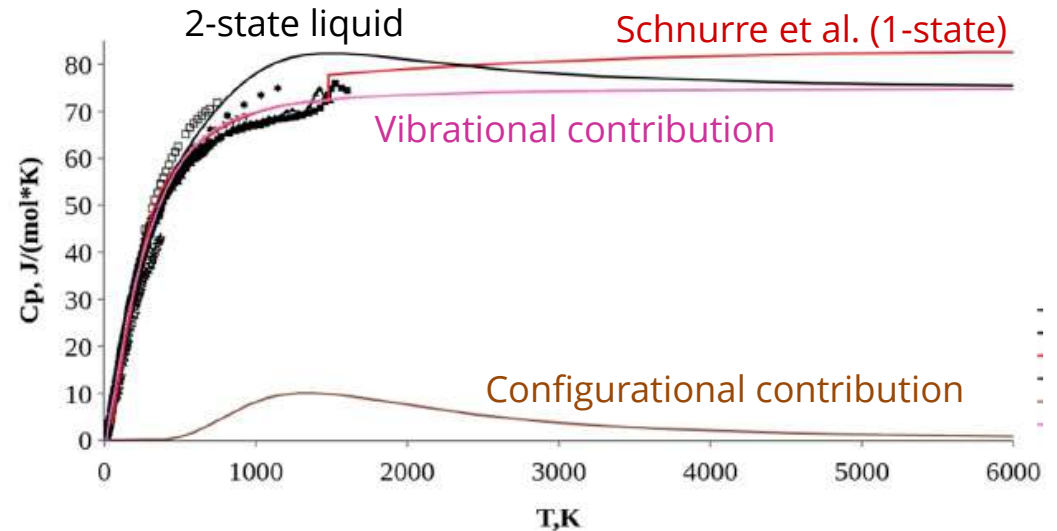
# Examples of 3<sup>rd</sup> generation descriptions of unary liquids

## Sn



G. Deffrennes, P. Faure, F. Bottin, J.M. Joubert, B. Oudot, Tin (Sn) at high pressure: Review, X-ray diffraction, DFT calculations, and Gibbs energy modeling, *J. Alloys Compd.* 919 (2022) 165675.

## SiO<sub>2</sub>



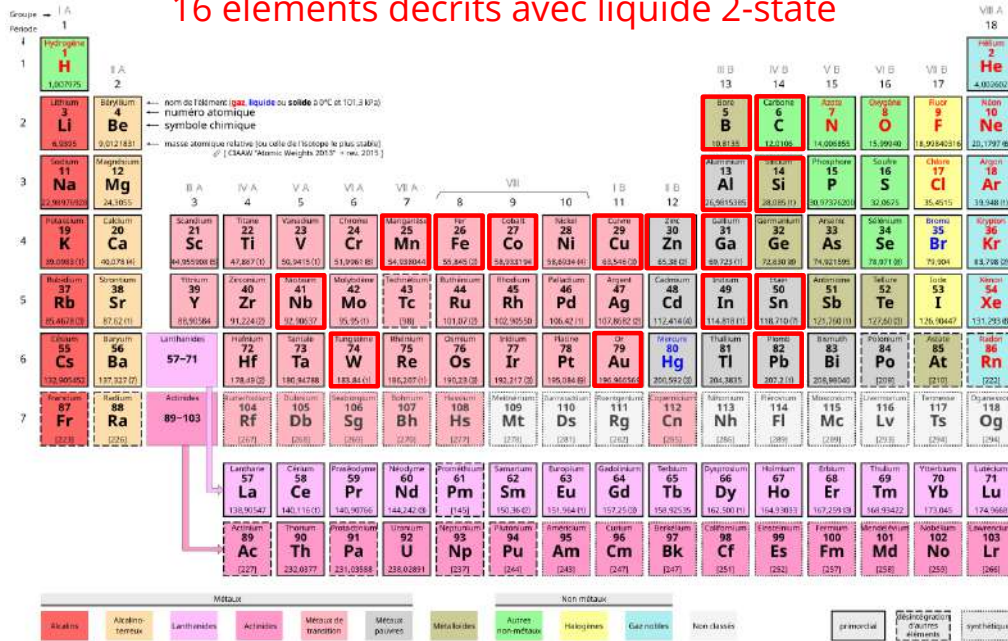
- The parameters are adjusted so that the peak of the two-state liquid corresponds to the glass transition temperature (around 1480 K)

I. Bajenova, A. Khvan, A. Dinsdale, A. Kondratiev, Implementation of the extended Einstein and two-state liquid models for thermodynamic description of pure SiO<sub>2</sub> at 1 atm, *Calphad Comput. Coupling Phase Diagrams Thermochem.* 68 (2020) 101716



# Conclusions

## 16 éléments décrits avec liquide 2-state



- Quelques oxydes simples :  $B_2O_3$ ,  $CaO$ ,  $SiO_2$ ,  $GeO_2$
- Quelques systèmes multiconstitués
  - Binaires : Al-C, Al-Zn, B-Fe, Pb-Sn, C-W
  - Ternaire : B-Fe-Nb
- Certaines de ces descriptions adoptent des choix de modélisation ou de paramétrisation discutables
- L'utilisation d'un modèle à 2 états régulier a été proposée
  - pour améliorer la capacité du modèle à représenter les informations expérimentales disponibles
  - pour pouvoir modéliser le polymorphisme liquide

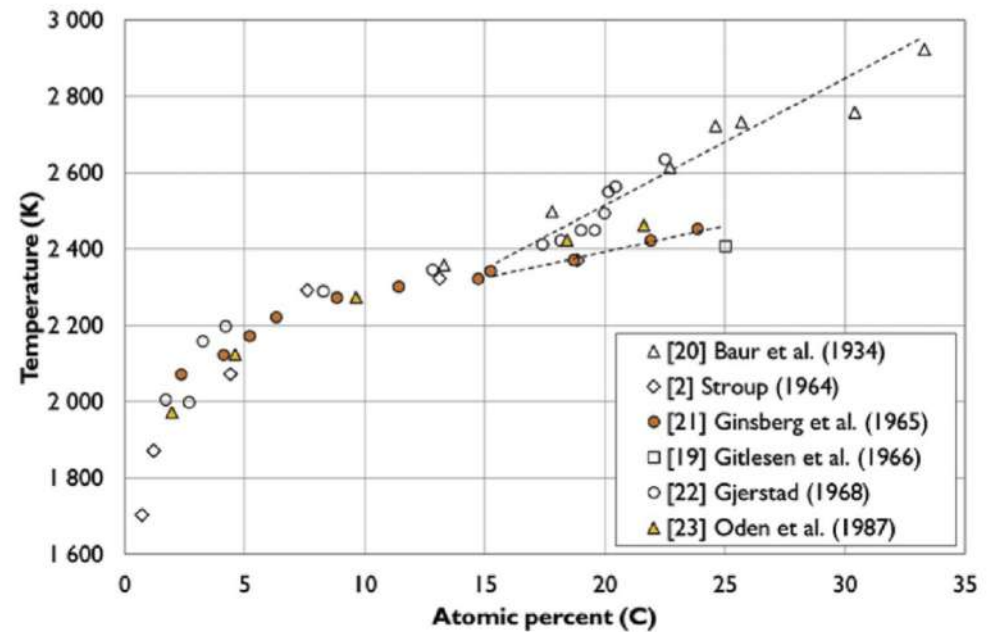
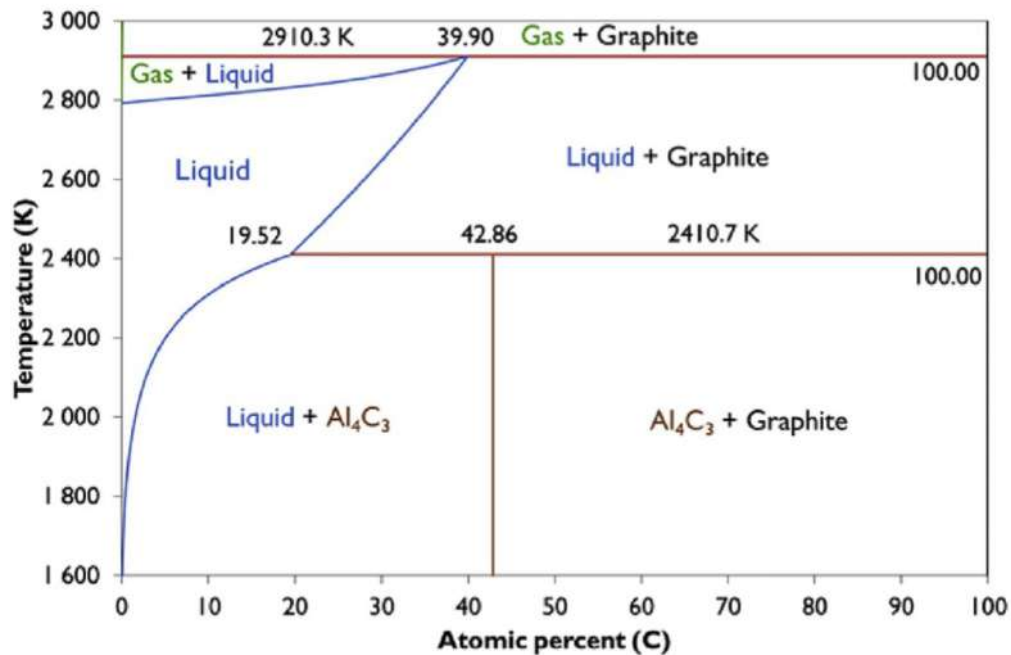
# Modeling chemical interaction



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# Modeling interaction : (Sub) regular solution



G. Deffrennes et al, Calphad 66 (2019) 101648.

# Modeling interaction : (Sub) regular solution

$$G^{Liq} = G^{ref} + G^{ideal} + G^{exc}$$

$$G_m^{Liq, ex} = x_{Al}x_C (L_{Al,C_0}^{Liq} + L_{Al,C_1}^{Liq} (x_{Al} - x_C))$$

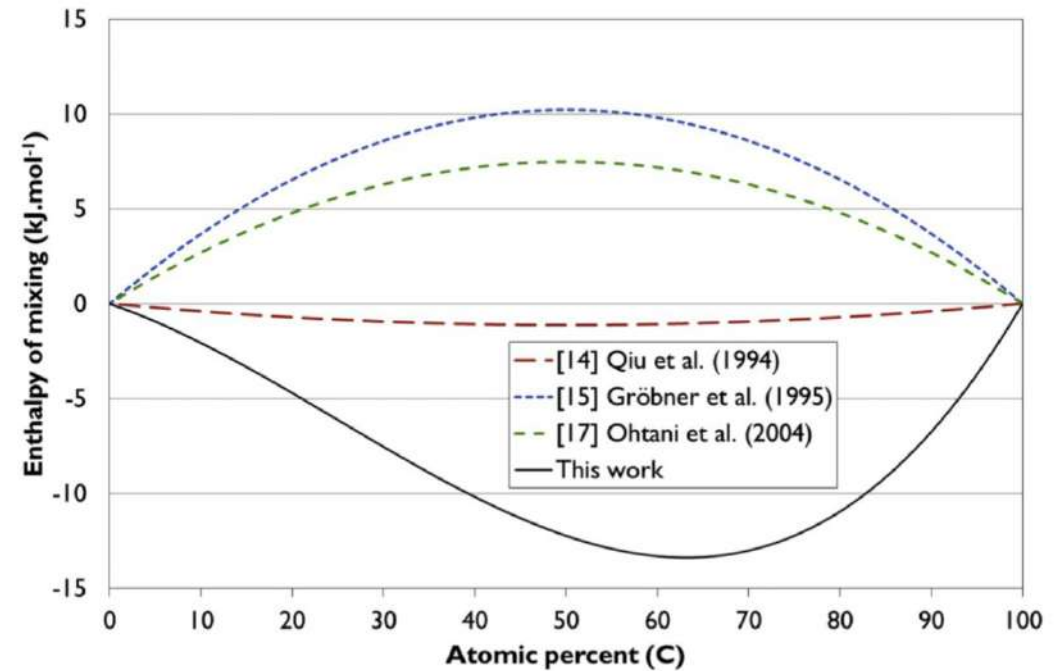
$${}^0L_{Al,C}^{Liq} = {}^0a_{Al,C}^{Liq} + {}^0b_{Al,C}^{Liq} T$$

$${}^1L_{Al,C}^{Liq} = {}^1a_{Al,C}^{Liq}$$

Liquid, Redlich-Kister, (Al, C)

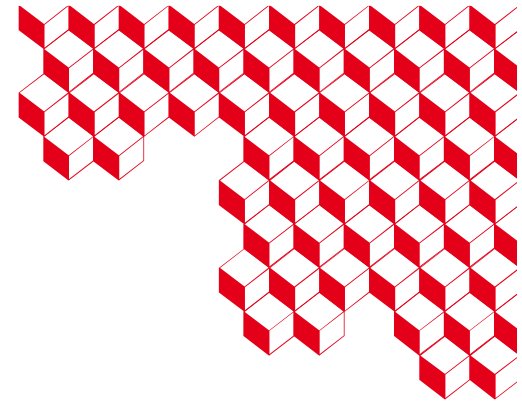
${}^0L_{Al,C}^{Liq}$	[14] Qiu et al. (1994)	-4426	-11.1007
	[15] Gröbner et al. (1995)	+40861.02	-33.21138
	[17] Ohtani et al. (2004)	+29910	-25.586
	This Work	-48892	+1.15
${}^1L_{Al,C}^{Liq}$	This Work	+32543	-

G. Deffrennes et al, Calphad 66 (2019) 101648.





isqs



## Modèle ionique pour décrire les liquides

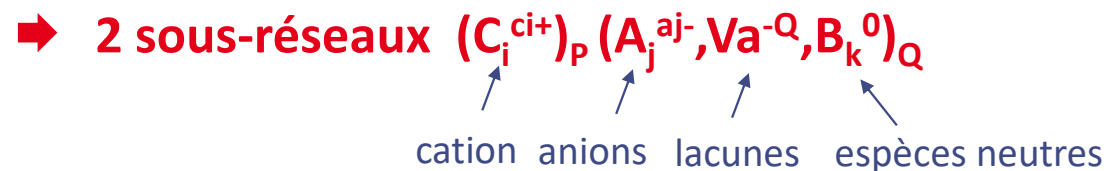
Christine Guéneau

Université Paris-Saclay, CEA, Service de Recherche en Corrosion et Comportement des Matériaux  
Gif-sur-Yvette, France

# Partially ionic two sublattice model



- ✓ Possibilité de décrire des liquides métalliques et non métalliques (oxydes, sulfures, chlorures ...)



- ➔ Introduction de lacunes chargées (-Q) pour décrire le liquide métallique  $(C_i^{c_i+})_p (Va^{-Q})_Q$
- ➔ La charge des lacunes (-Q) varie avec la composition pour maintenir la relation d'électroneutralité

$$P = \sum a_j y_{A_j} + Q y_{Va}$$

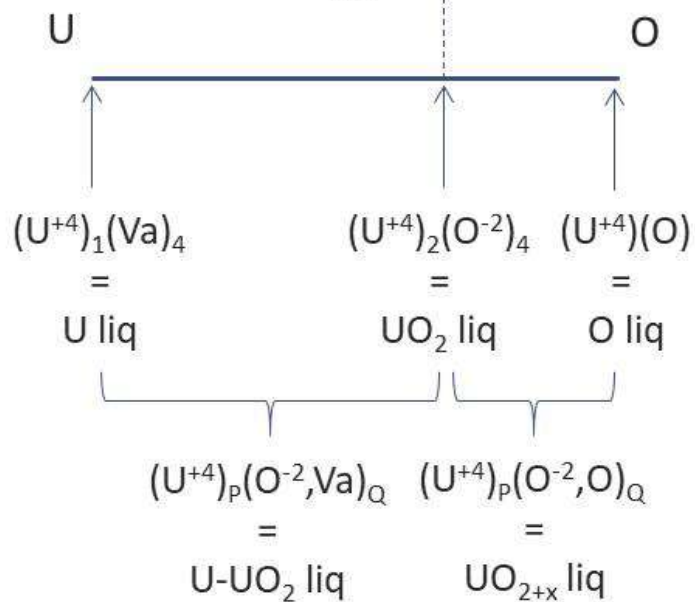
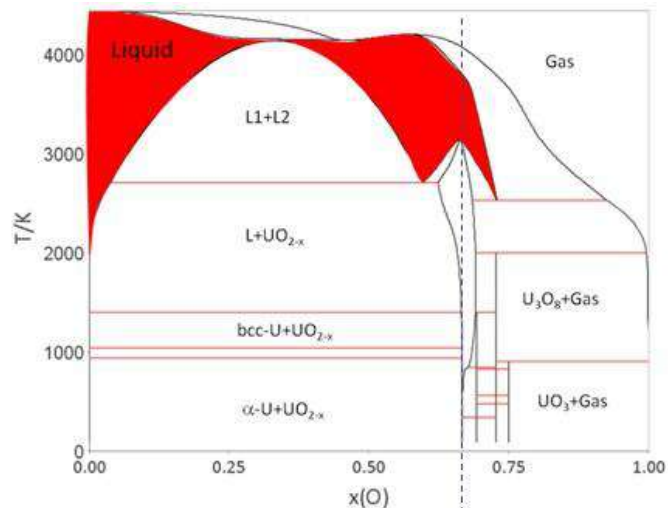
$$Q = \sum c_i y_{C_i}$$

- ➔ L'ordre à courte distance est pris en compte par l'introduction d'espèces chargées

Exemple:  $(Ba^{+2})(MoO_4^{-2})$



# Exemple: Système U-O



➔ Two ionic sublattice model  $(U^{+4})_p(O^{-2}, Va^{-Q}, O)_Q$

$$P = 2y_{O^{-2}} + Qy_{Va^{-Q}}$$

$$Q = 4$$

P = Charge moyenne du sous-réseau 2

Q = Charge moyenne du sous-réseau 1

$$G_m^{Liq} = y_{U^{+4}}y_{O^{-2}}G_{(U^{+4})_2(O^{-2})_4}^0 + y_{U^{+4}}y_{Va}G_{(U^{+4})_1(Va)_4}^0 + y_{U^{+4}}y_OG_O^0 + QRT(y_{O^{-2}} \ln y_{O^{-2}} + y_{Va} \ln y_{Va} + y_O \ln y_O) + G_m^{Excess}$$

← Endmembers

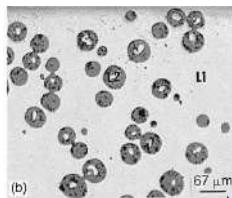
← Paramètres d'interaction

Aucune donnée sur le liquide  
Excepté le Cp de UO<sub>2</sub> liquide

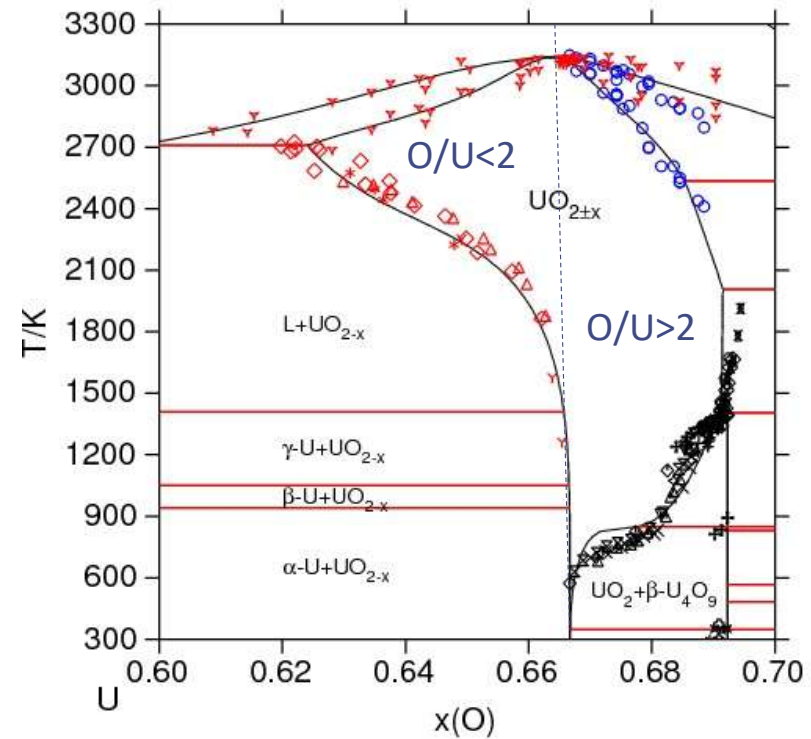
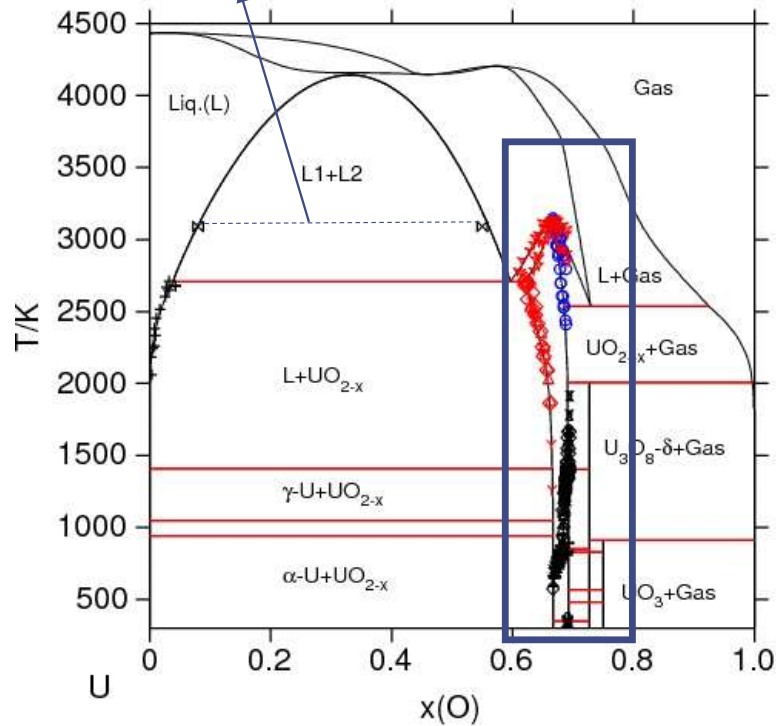




# Diagramme de phase U-O



L1+L2



⇒ T fusion de  $\text{UO}_2$  très élevée = 3120 K  
 ⇒ T solidus / liquidus ↘ avec x dans  $\text{UO}_{2\pm x}$   
 ⇒ **Lacune de miscibilité à l'état liquide (L1+L2)**

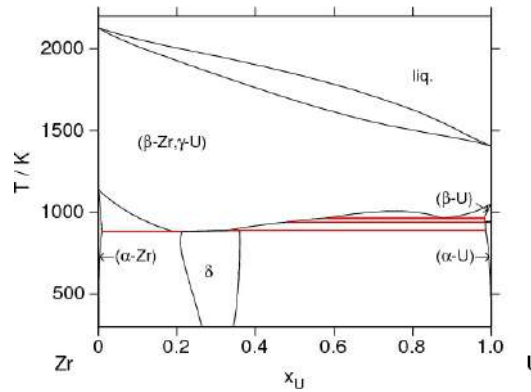
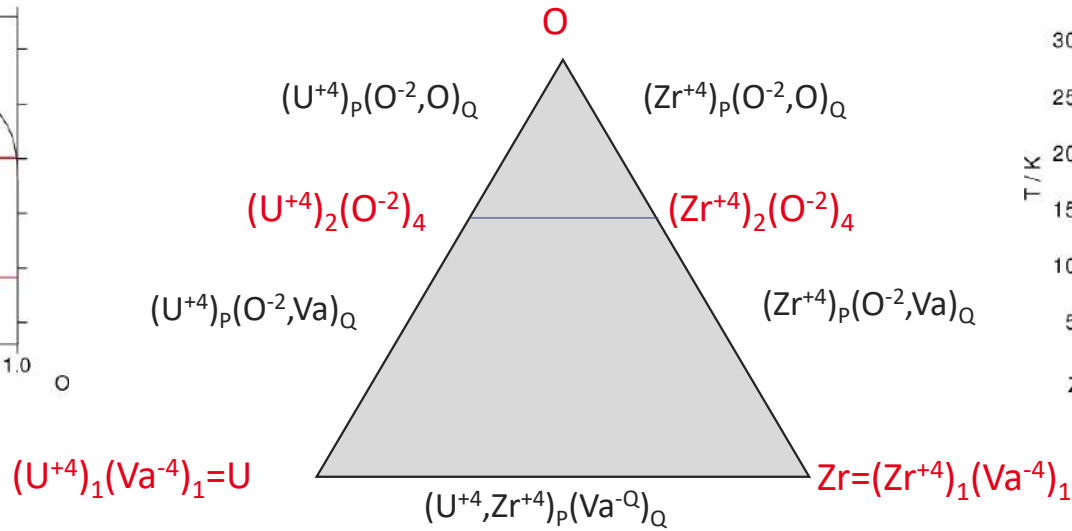
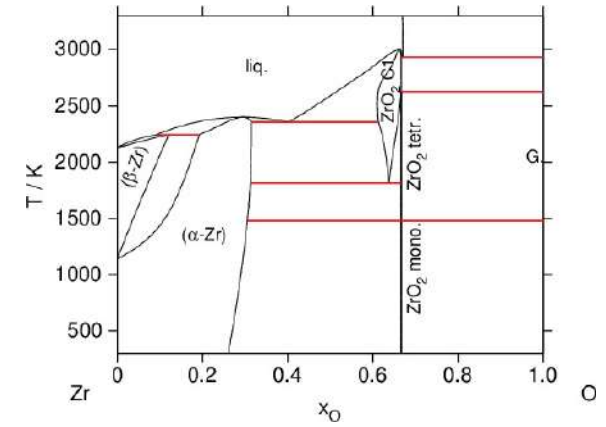
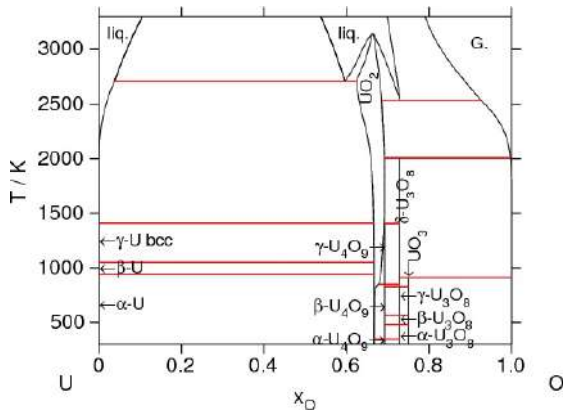


[Guéneau et al, J. Nucl. Mater. 254 (1998) 158  
Guéneau et al, J. Nucl. Mater. 419 (2011) 145]

# Exemple: Système U-Zr-O



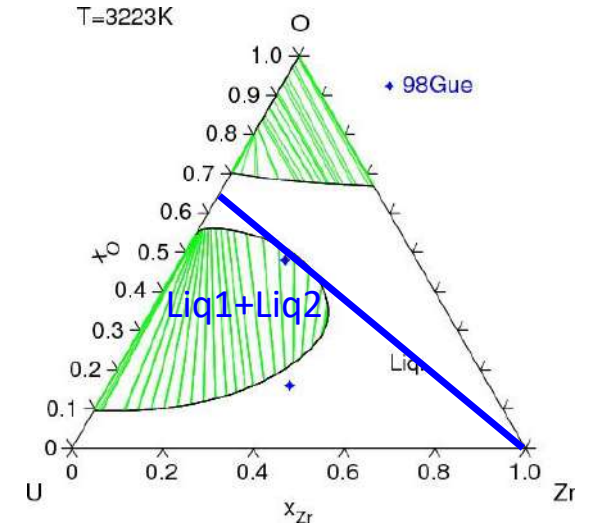
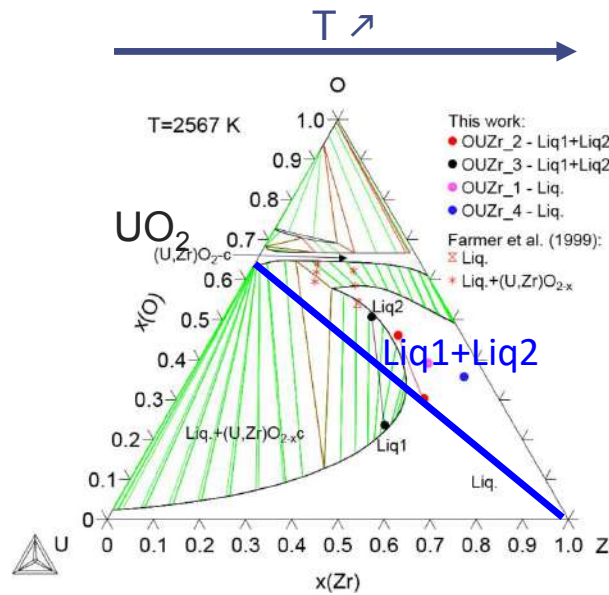
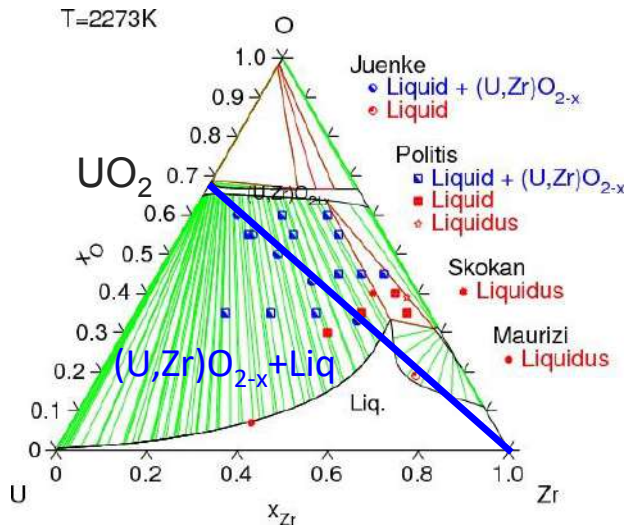
➔ Model  $(U^{+4}, Zr^{+4})_p(O^{-2}, Va^{-Q}, O)_Q$



# Système U-O-Zr ➔ Interaction $\text{UO}_2$ /Zr

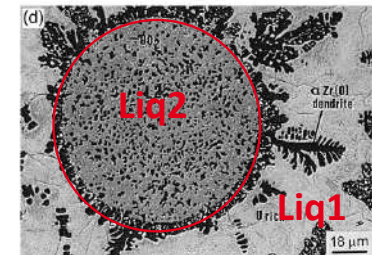
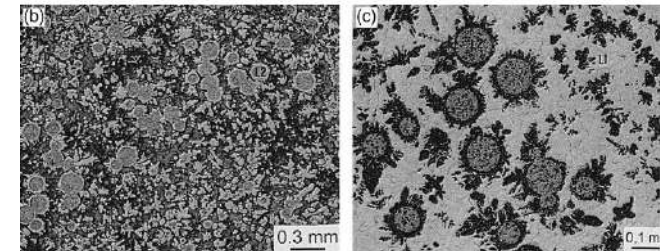
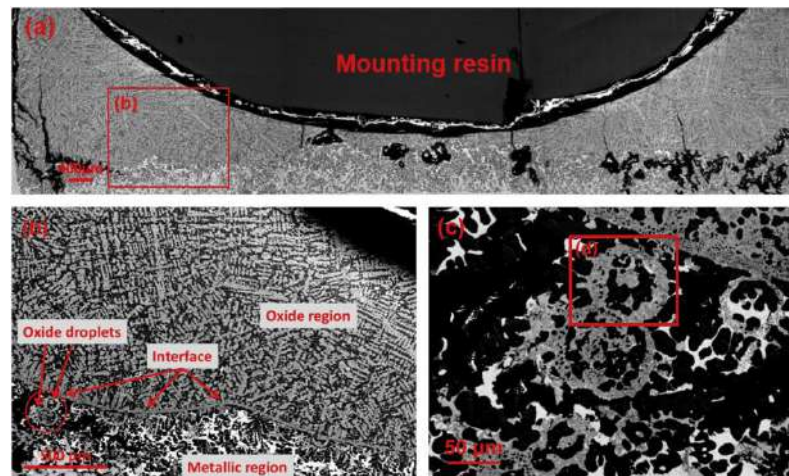


Model  $(\text{U}^{+4}, \text{Zr}^{+4})_p(\text{O}^{-2}, \text{Va}^{-Q}, \text{O})_Q$



- ✓ Interaction  $\text{UO}_2$ /Zr
- T=2273 K:  $(\text{U,Zr})\text{O}_{2-x}$  + Liq
- T=2567 K: Liq 1 metal + Liq 2 ox
- ➔ Lacune de miscibilité à l'état liquide

[Thèse Andréa Quaini (2015),  
Quaini et al, JNM 501 (2018) 104,  
Guéneau et al, J. Nucl. Mater. 254  
(1998) 158]



Journée de prospective sur la physicochimie des liquides à Haute Températures  
29 Novembre 2024, Paris

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# Using machine learning to study liquids

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Guillaume Deffrennes

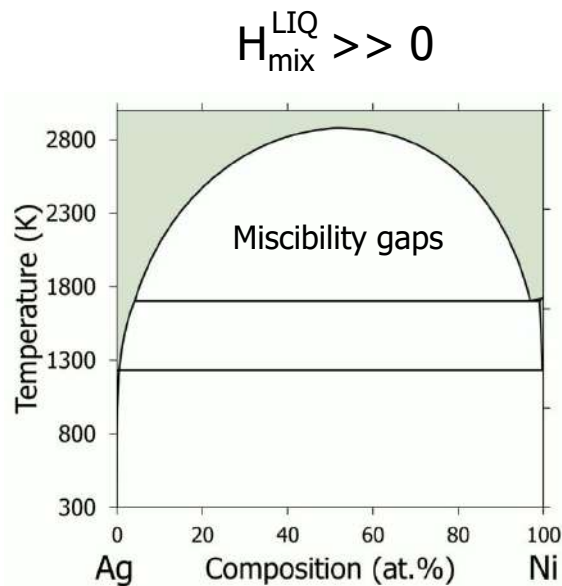
CNRS, Univ. Grenoble Alpes, Grenoble INP, laboratoire SIMaP



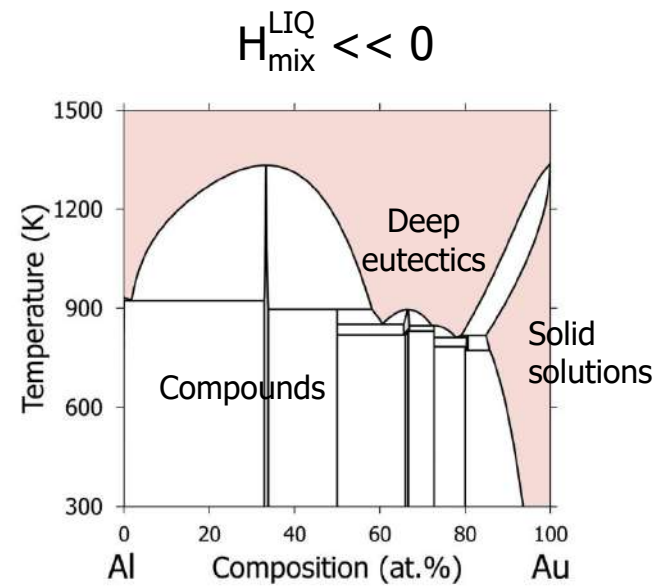
# Case study of the enthalpy of mixing in the liquid

$H_{\text{mix}}^{\text{LIQ}}$  is :

- ... essential for modeling the stability of liquids
- ... used in empirical rules, e.g., to design metallic glasses Takeuchi *et al.*, Mater. Trans., 46 (2005)
- ... correlated to phase diagrams Miedema *et al.*, Physica 100B (1980)



Liu *et al.*, J. Electron. Mater. 37 (2008)



Li *et al.*, J. Alloys Compd. 385 (2004)

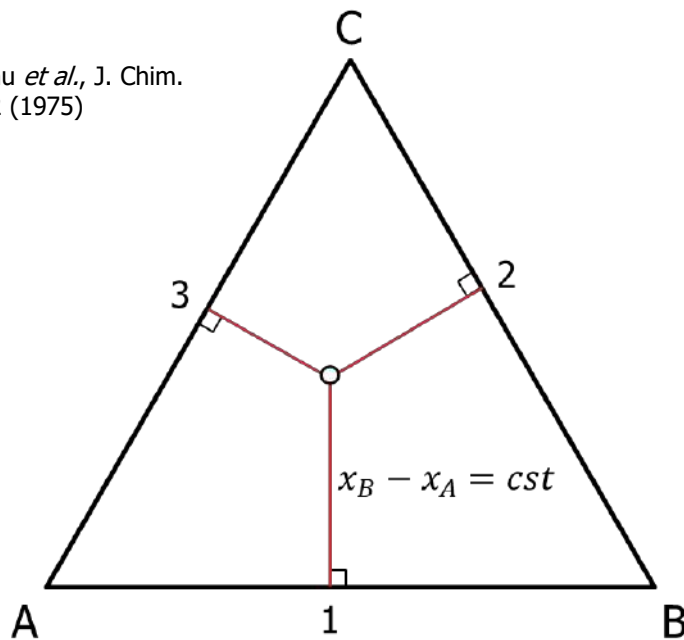


# Extrapolation from binary to multicomponent liquids

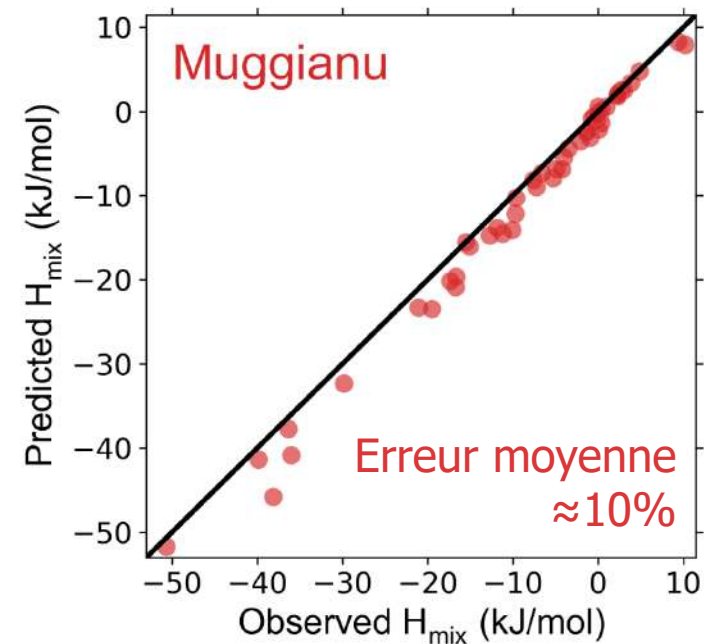
## Muggianu's model

$${}^{bin}H_{mix} = x_A x_B L_{AB(1)} + x_B x_C L_{BC(2)} + x_C x_A L_{CA(3)}$$

Muggianu *et al.*, J. Chim. Phys. 72 (1975)



Performance on 52 ternary near-equimolar **metallic** liquids



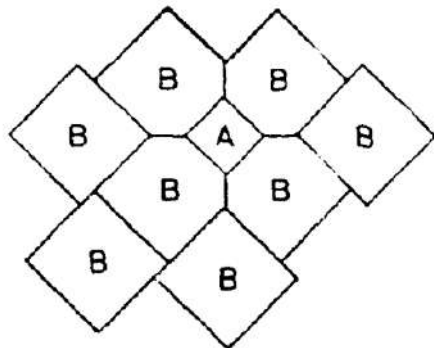
Deffrennes *et al.*, Calphad 87 (2024)

→ Focus on binary liquids

# Predictions in binary liquids from Miedema's model

The atomic cell model

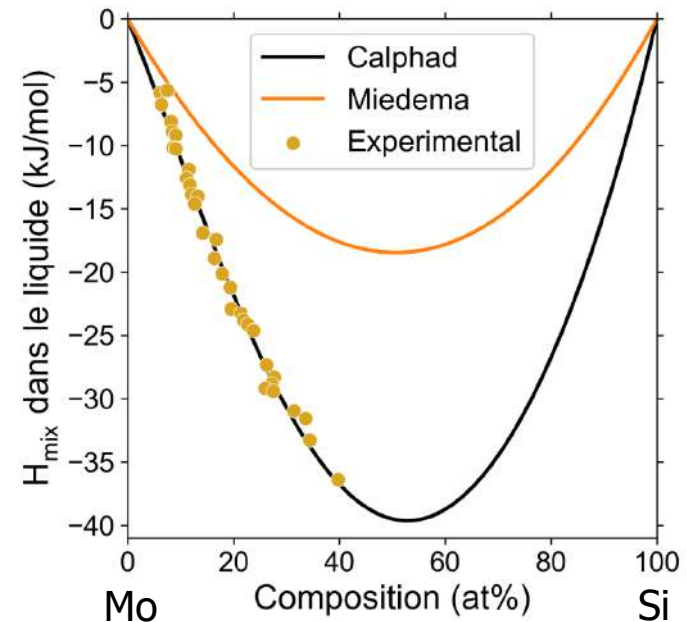
Miedema *et al.*, Physica 103B (1981)



$\approx$  electronegativity

$$H_{mix}^{LIQ} \propto A (-P\Delta\phi^2 + Q(\Delta n_{ws}^{1/3})^2)$$

Area of A-B interface    Electronic density at the cell boundary



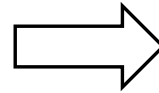
Geng *et al.*, Calphad 34 (2010)

- What accuracy can be expected from Miedema's model?
- Can we correct it using machine learning?

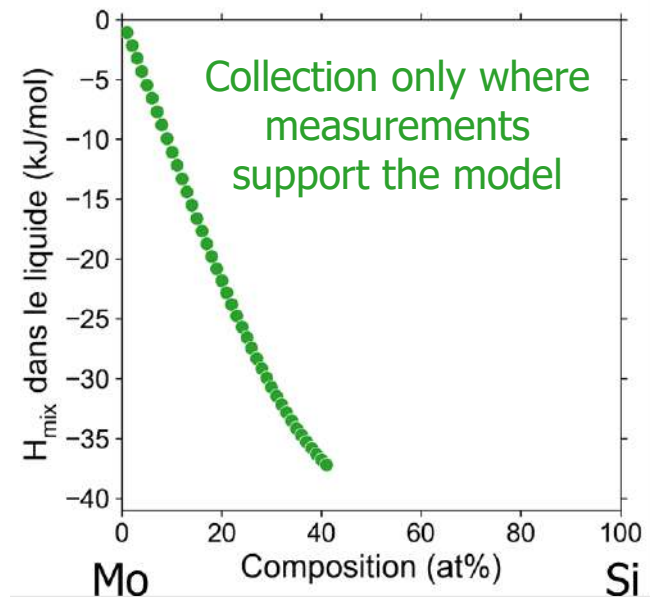
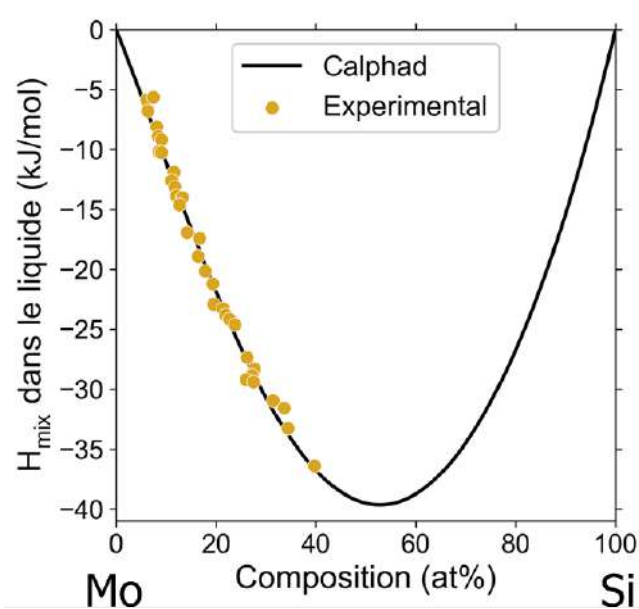


# Data collection

CALPHAD assessments



Dataset

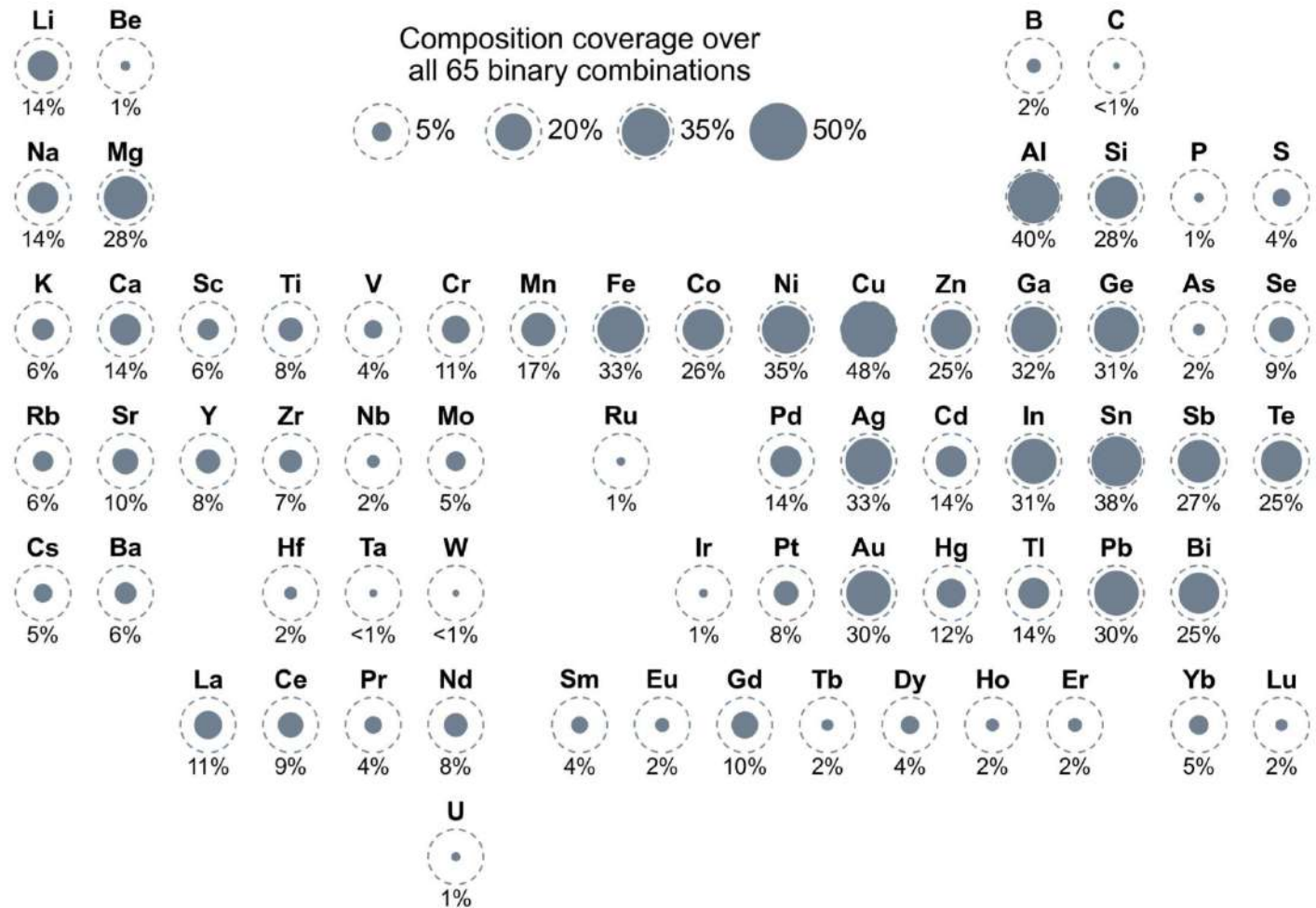
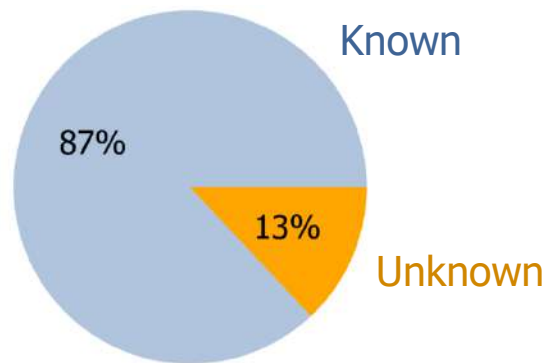


- Review of  $\sim 1000$  Calphad assessments
- Reliable data found in 375 binary systems

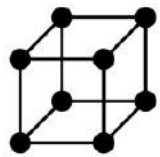
# Dataset

Deffrennes *et al.*, Calphad 87 (2024)

Amount of data per element

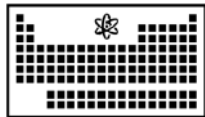


$$H_{\text{mix}}^{\text{Réal}} - H_{\text{mix}}^{\text{Miedema}} = f_{\text{ML}} (\text{features})$$



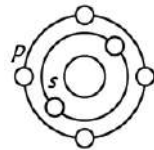
### Physico/chemical properties

Molar volume (at 300K)  
Thermal conductivity (at 300K)  
Density (at 300K)



### Periodic table

Atomic number  
Mendeleev number  
Row  
Column



### Electronic properties

Valence electron  
Unfilled valence orbitals  
First ionization energy  
Polarizability  
Electronegativity



### Atomic properties

Atomic weight  
Atomic radius  
Covalent radius

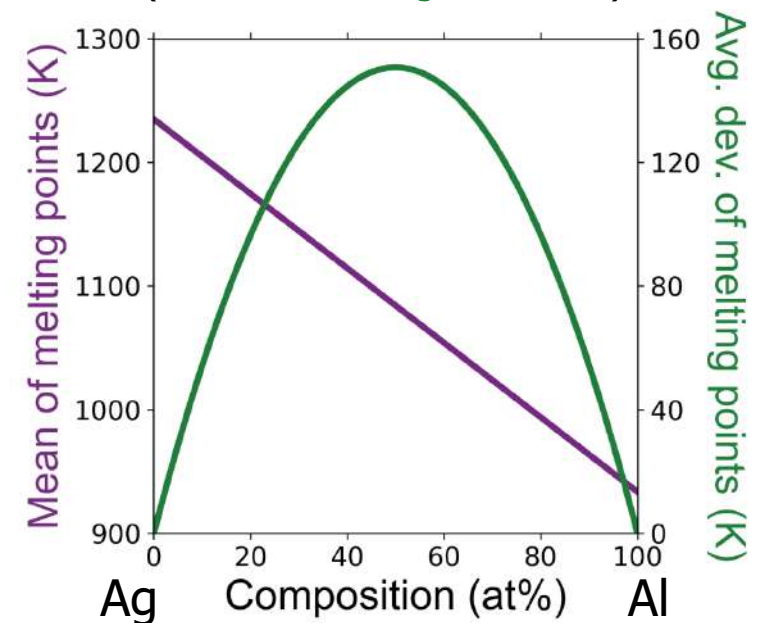


### Thermodynamic properties

Boiling point  
Melting point  
Heat of vaporization  
Enthalpy and entropy of fusion (at  $T_m$ )  
Enthalpy and entropy of liquid (at  $T_m$ )  
Enthalpy and entropy of solid (at  $T_m$ )  
Heat capacity of solid, liquid and fusion (at  $T_m$ )  
Heat capacity and entropy (at 300K)

Features obtained from the composition weighted properties of the pure elements

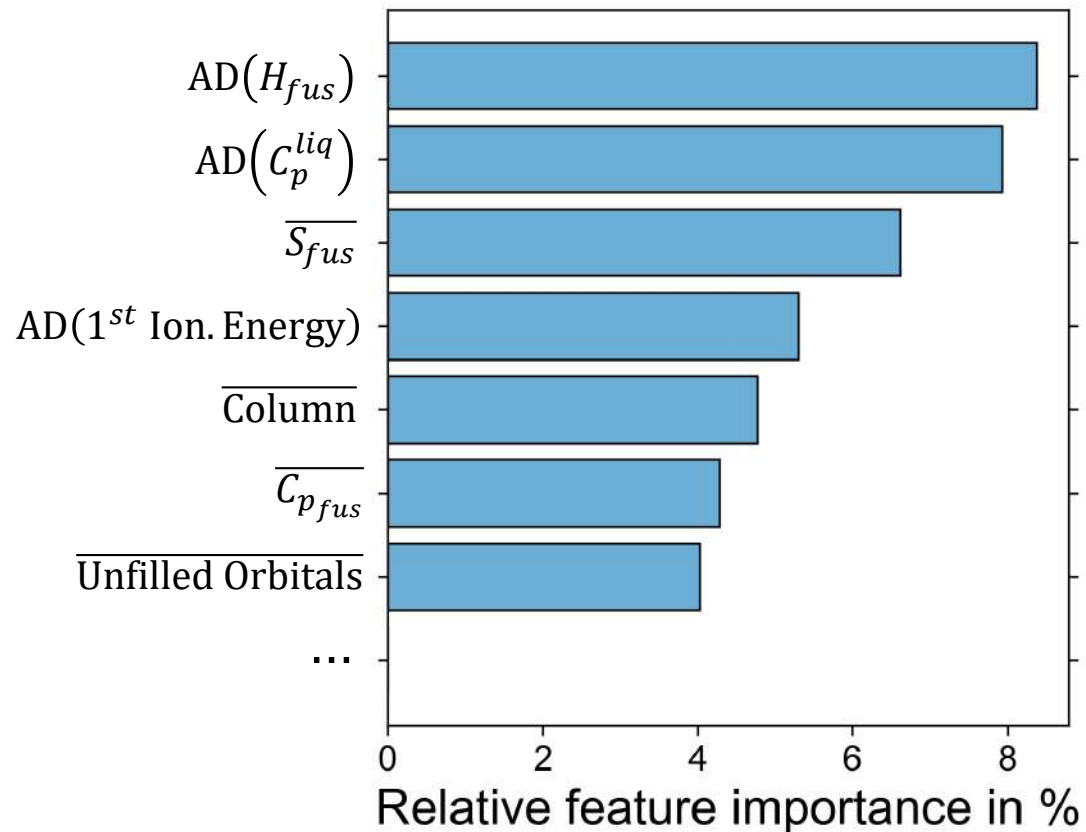
(mean and average deviation)



$$x_A |T_A - \bar{T}| + x_B |T_B - \bar{T}|$$

# Feature importance

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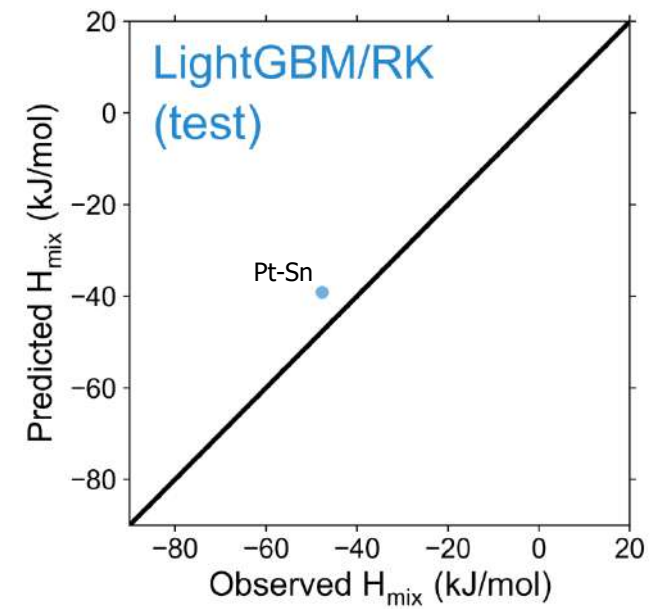
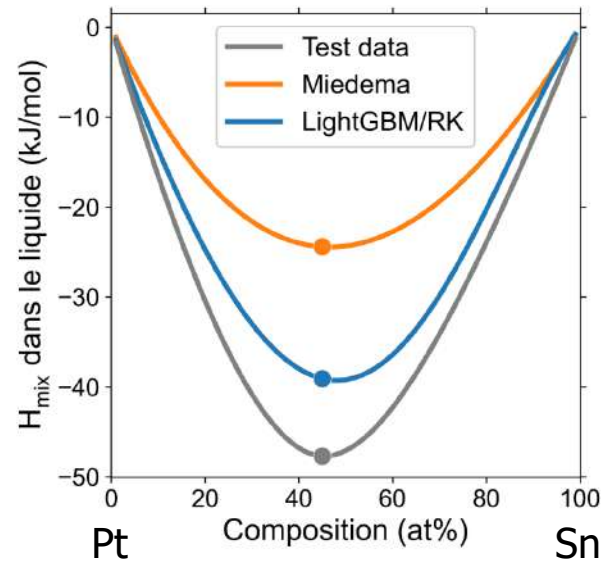
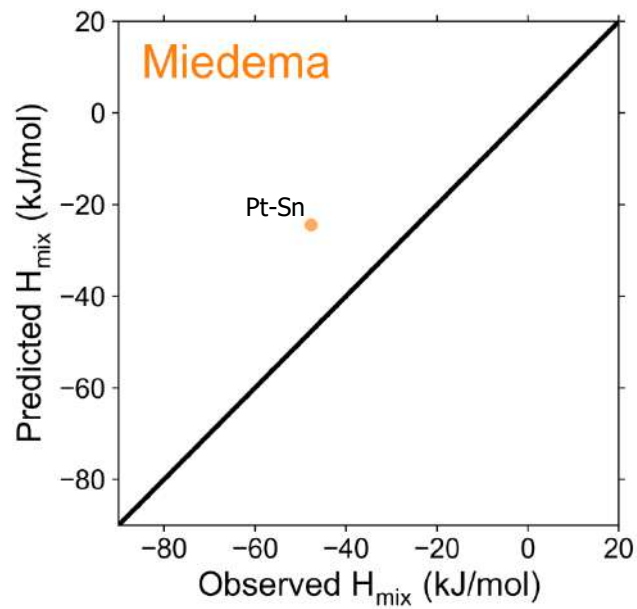


Can be useful to establish empirical laws

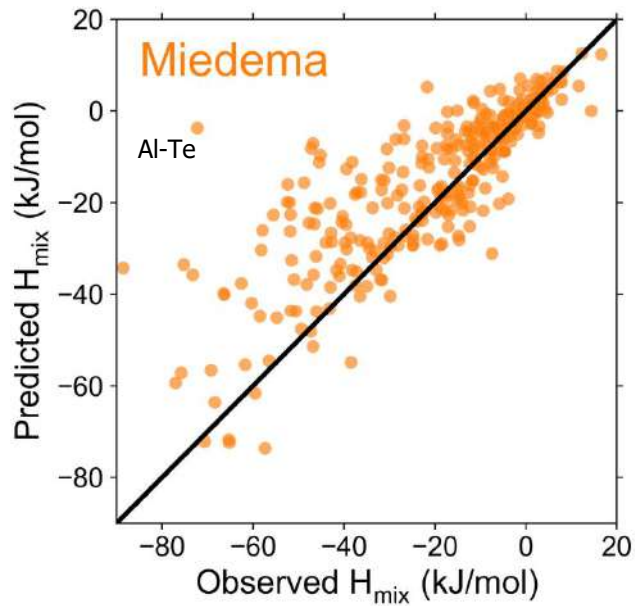
e.g.: Vazquez *et al.*, npj comput. mater. 68 (2023)

AD: average deviation

# Performances



# Performances

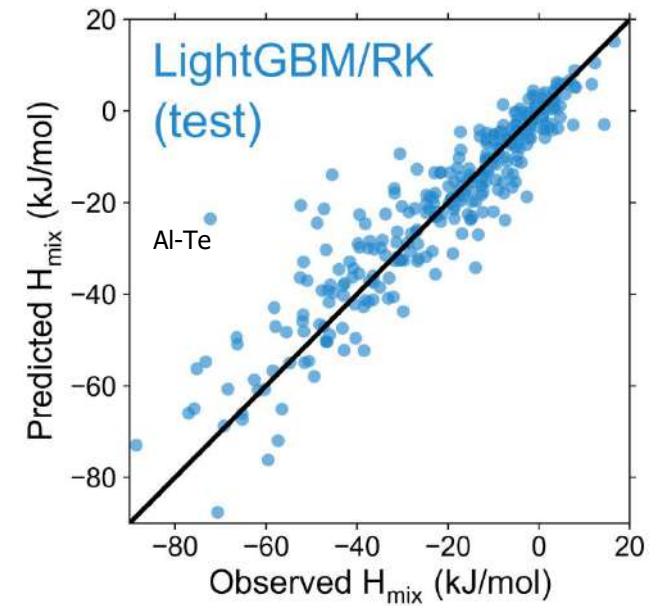


31%

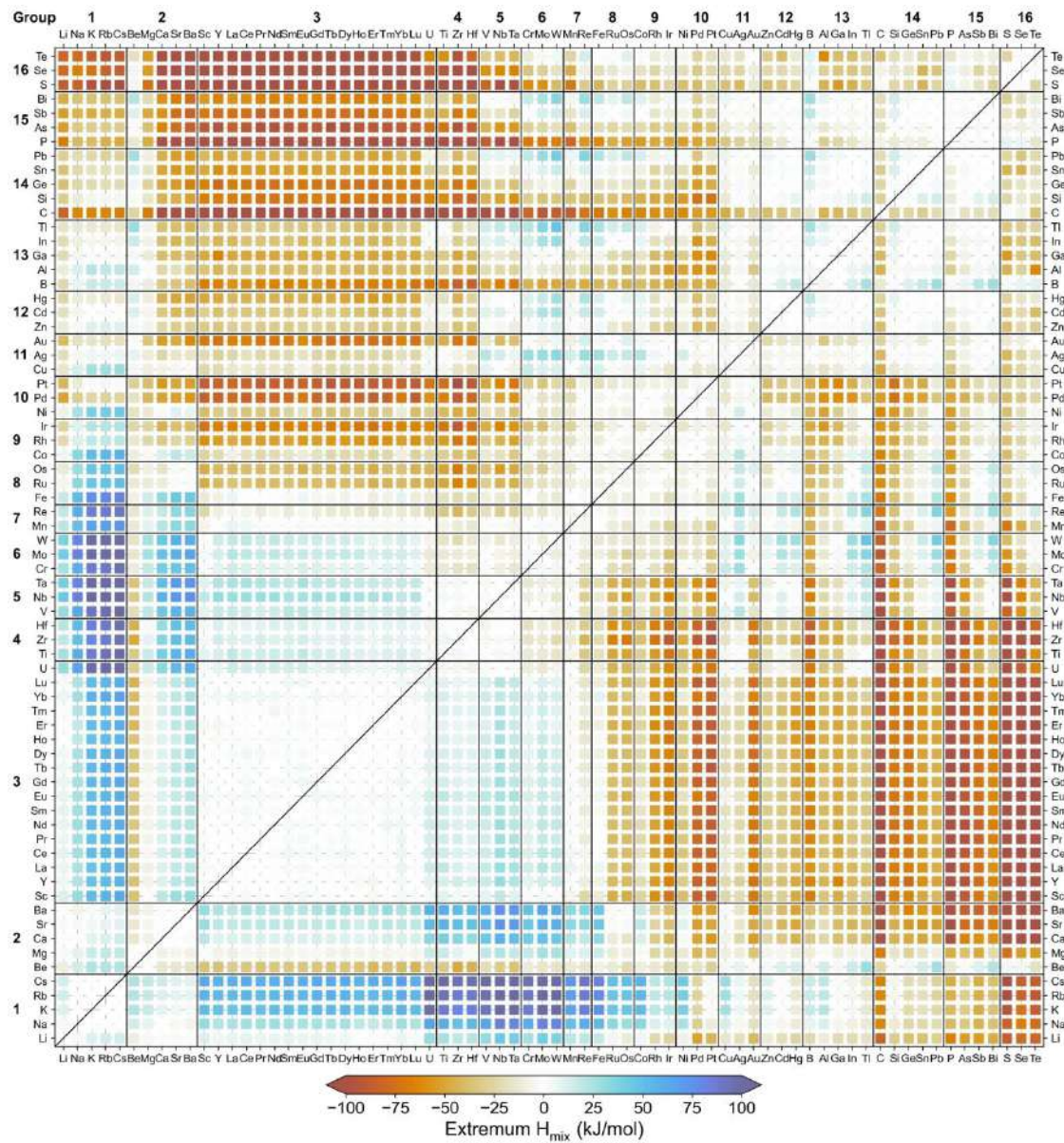
Mean Absolute % error  
(on data > 15 kJ/mol in abs. value)

$$= \frac{100}{n} \sum_n \frac{|H_{mix}^{True} - H_{mix}^{Pred}|}{H_{mix}^{True}}$$

18%



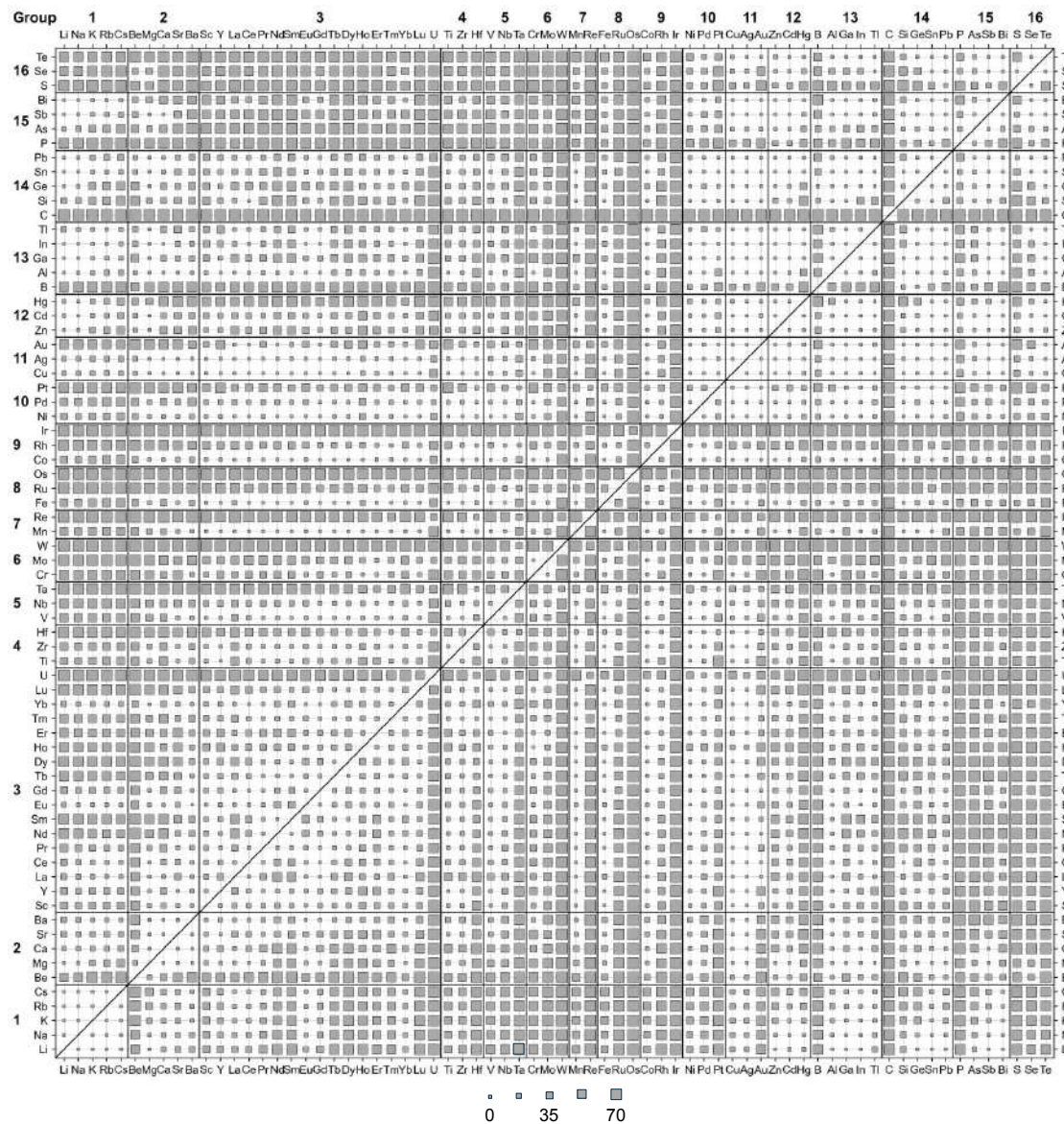




## Predictions in 2415 binary liquids between 70 elements

Deffrennes *et al.*, Calphad 87 (2024)





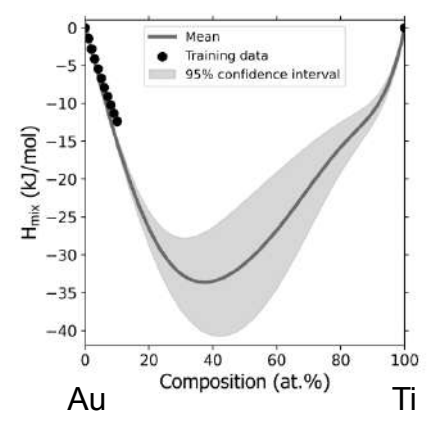
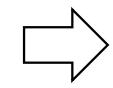
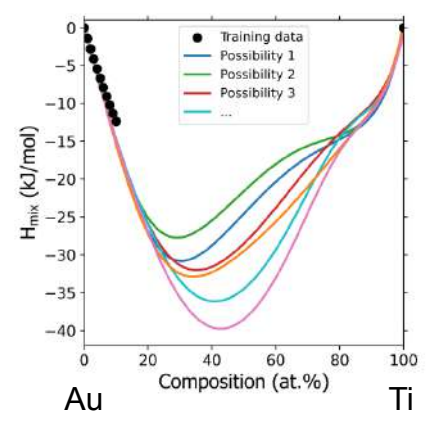
Maximum variance of the Gaussian Process model (kJ/mol)<sup>2</sup>

Where is new data needed the most?  
 → Active learning

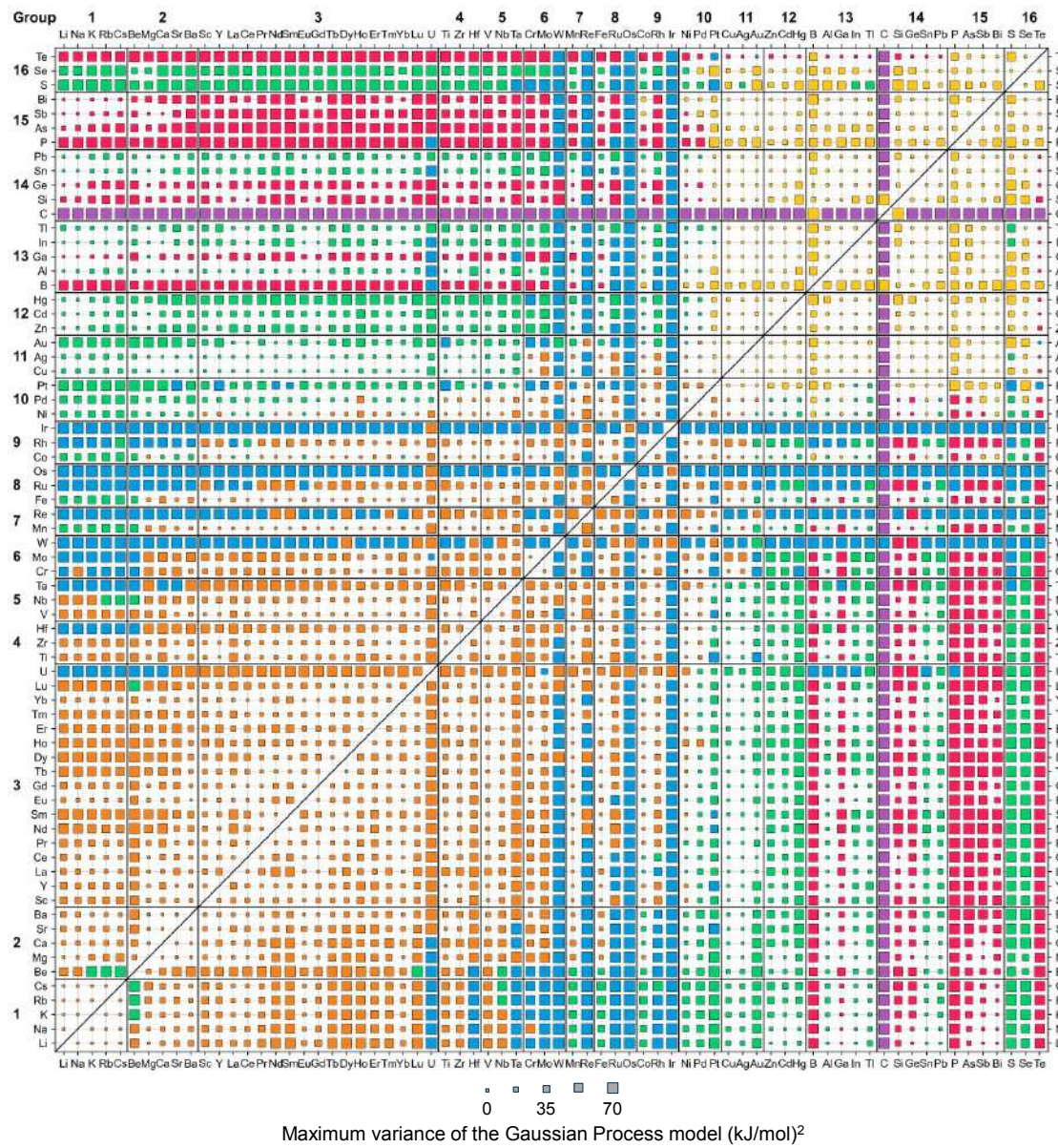
Work of Quentin Bizot  
 (post-doc)



### Gaussian Process







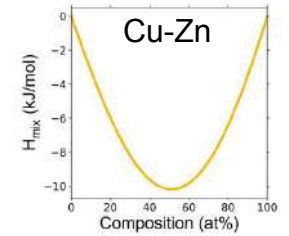
# Clustering for a better understanding

- Column (mean & avg. deviation)
- $C_{p,liq}$  (mean & avg. deviation)
- $C_{p,fus}$  (avg. deviation)
- $H_{fus}$  fus (avg. deviation)
- $S_{fus}$  fus (mean & avg. deviation)
- 1<sup>st</sup> ion. energy (avg. deviation)
- Density (avg. deviation)

## K-means on 10 Features

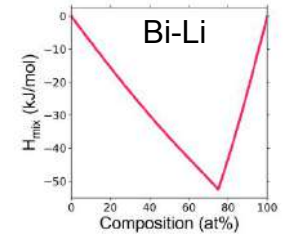
### Orange & Yellow (Similar groups)

- Some data
- High accuracy



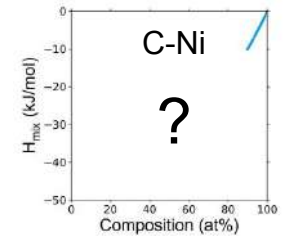
### Green & Red (Different groups)

- Some data
- Low accuracy due to SRO

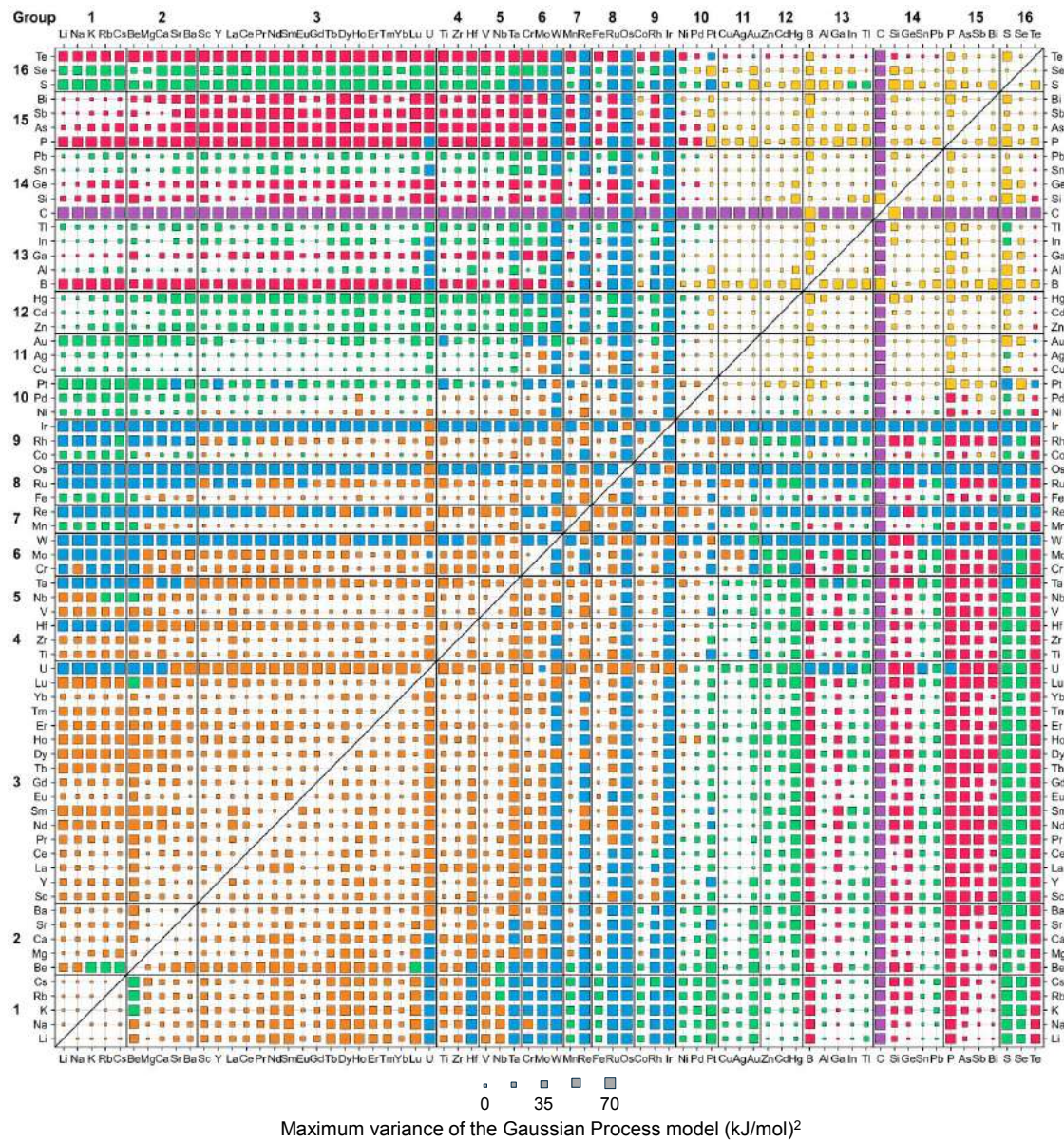


### Purple & Blue (Refractory elements)

- Little data
- Low accuracy

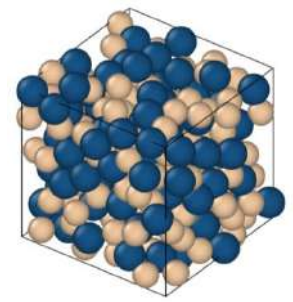






Data acquisition for refractory alloys  
(work in progress)

Ab initio Molecular Dynamics



**Ir-Si**  
(equimolar)

# Conclusion

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Machine learning can help with:

- Estimations
- Data acquisition
- Reasoning and establishing empirical laws
- ... and more !

**Thank you for your attention !**

guillaume.deffrennes@cnrs.fr

# Conclusion & Outlook

## Calphad is a success story since 1970

- Large multicomponent databases available (commercial / public)
- Large variety of applications
- Base of ICME

## The future

- Third generation description & two-state model
- Integration of DFT / AIMD generated data
- New insights by ML / AI
- Still (desperately) needed : high temperature phase equilibria data & experimental thermodynamic properties
- Challenges
  - Modeling Metal - Oxide / Salt / ... equilibria & phase diagrams
  - Extrapolation to high temperatures & pressure dependence of condensed phases