

Surfaces and Textures

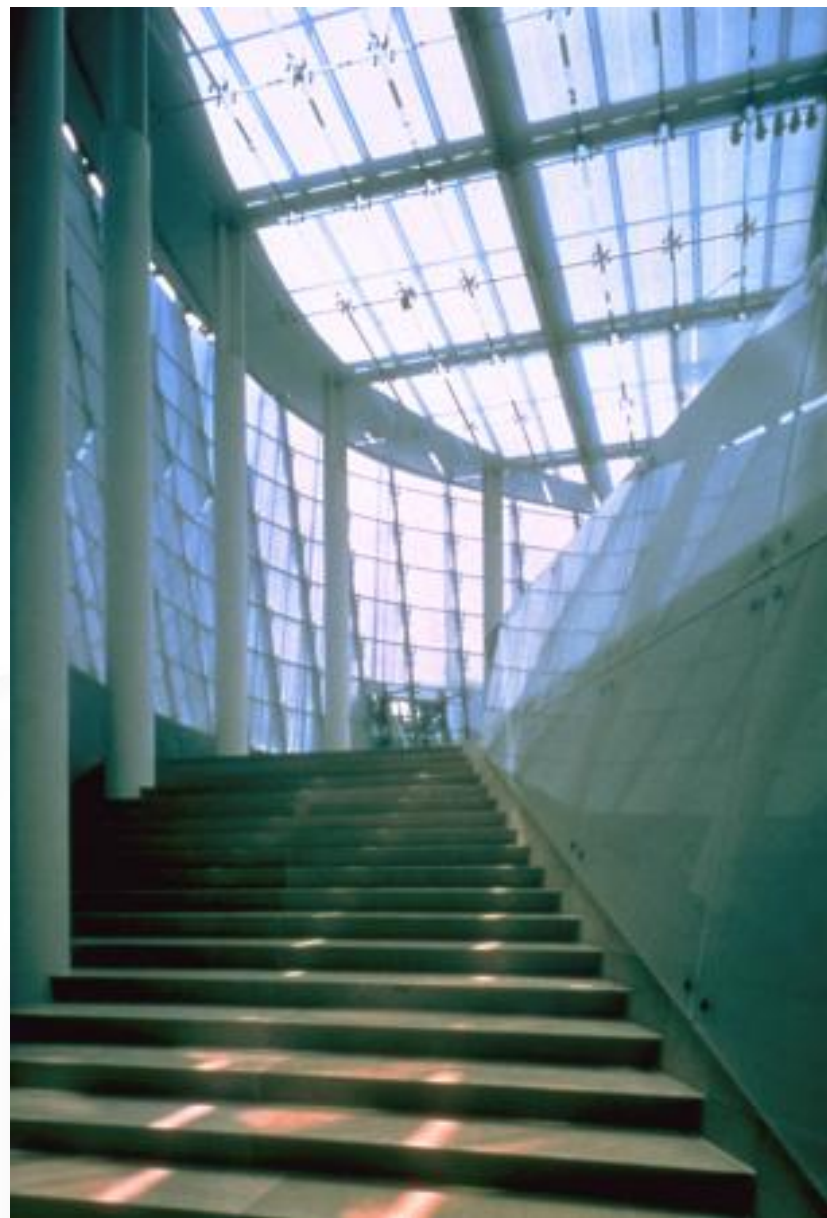
Nov 2010

L. Alzate, F. Guillemot, A. Letailleur,
D. Dalmas, J. Teisseire, S. Grachev,
E. Sondergard, E. Barthel



Silicate glasses are exceptional materials

- transparent
- stiff, hard
- experience... a glass transition
- mildly reactive surface



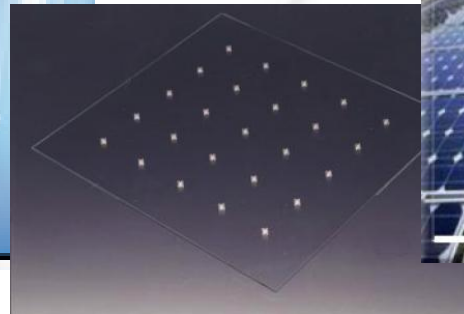
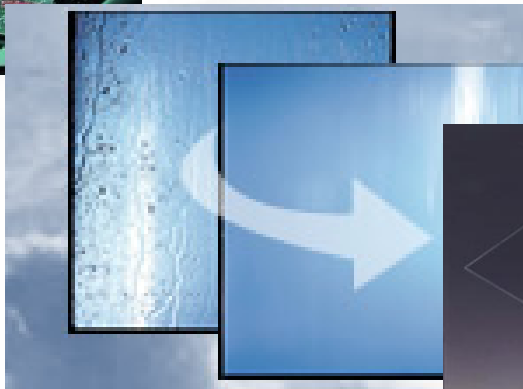
Saint-Jérôme
Albrecht Dürer



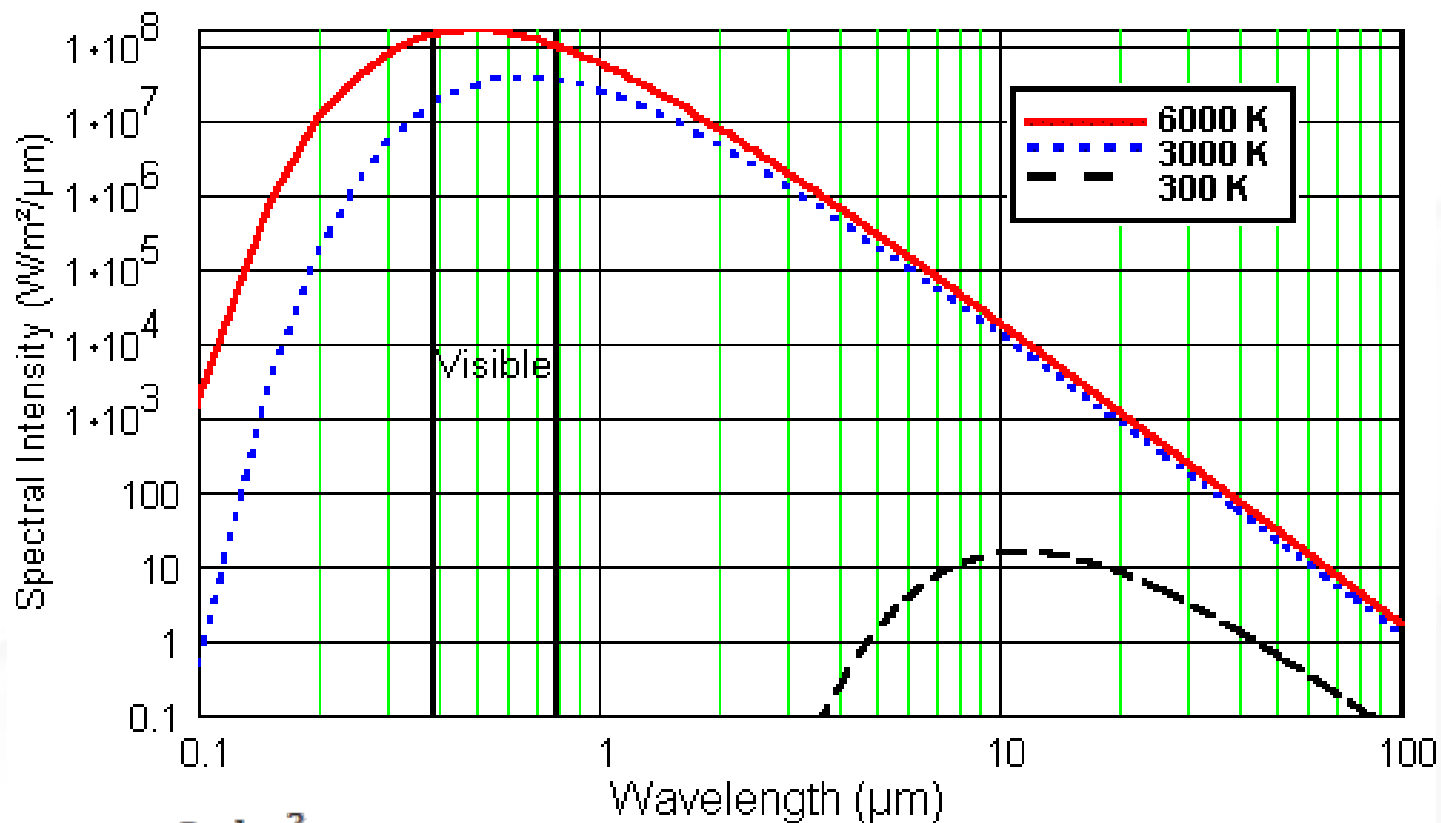
Surface Modification – why ?

Functionalization

- *optics*
- *wetting, contact, adhesion*



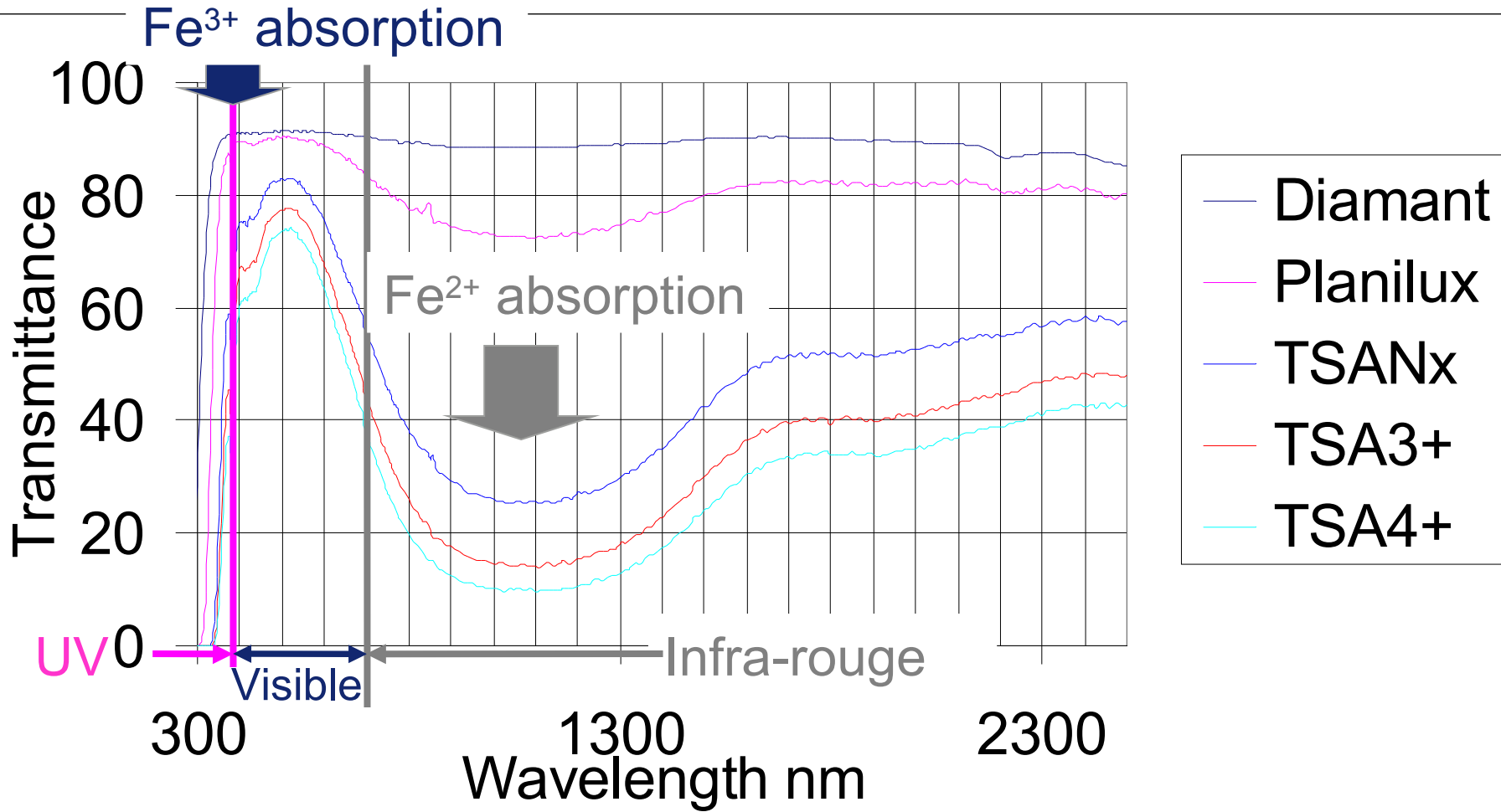
Blackbody radiation



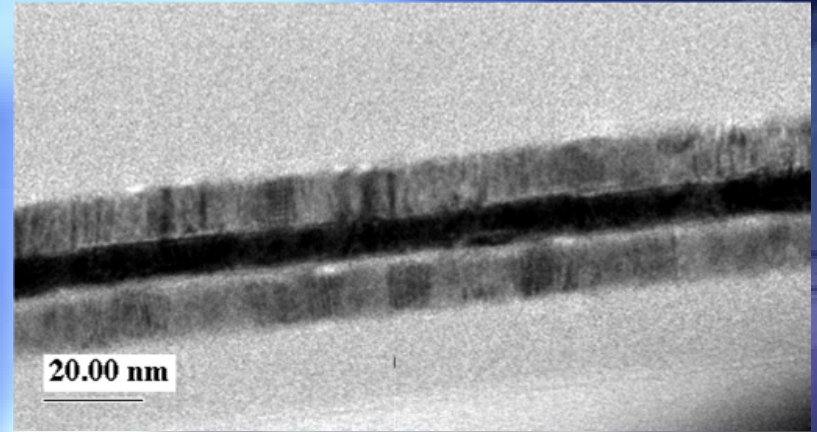
$$F(\lambda) = \frac{2\pi hc^2}{\lambda^5 \left(\exp\left(\frac{hc}{k\lambda T}\right) - 1 \right)}$$

www.pvcdrom.pveducation.org

Adjustment of the optical properties and of the solar energy transmission of the glass



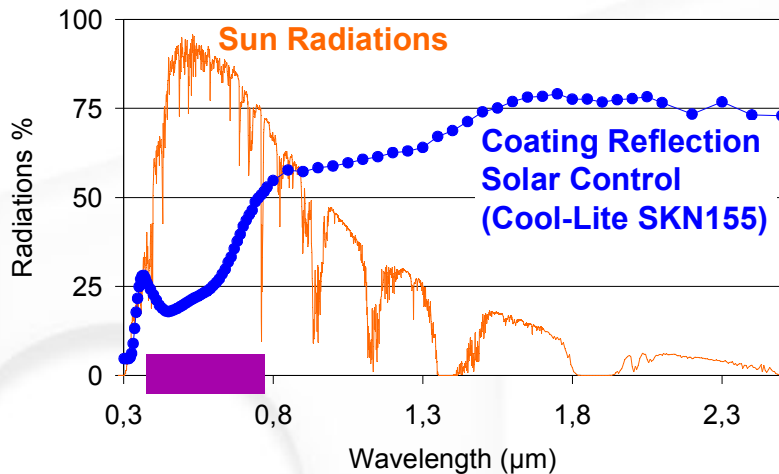
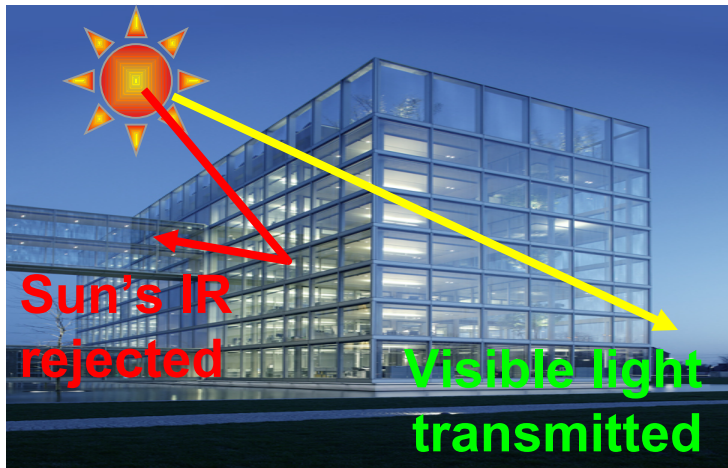
M.-H. Chopinet



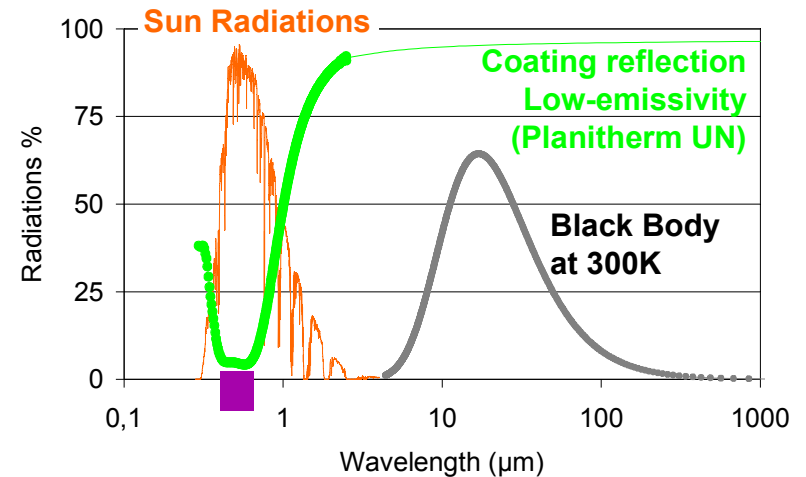
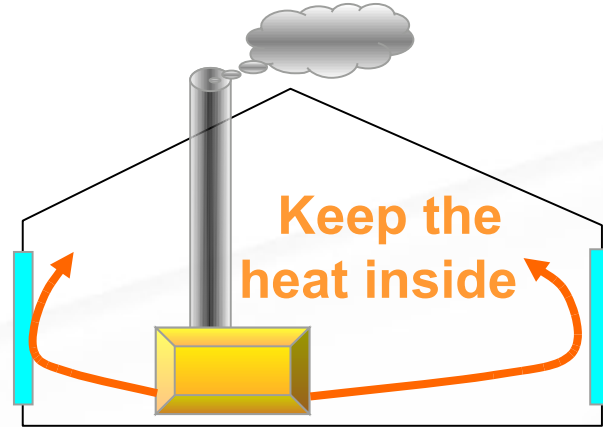
Solar Control

Two functions to reduce heat transfer due to radiations

Solar Control



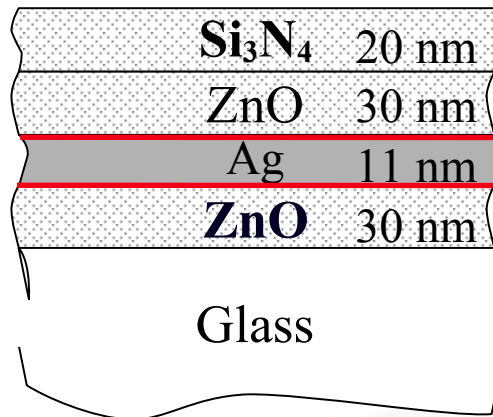
Low Emissivity



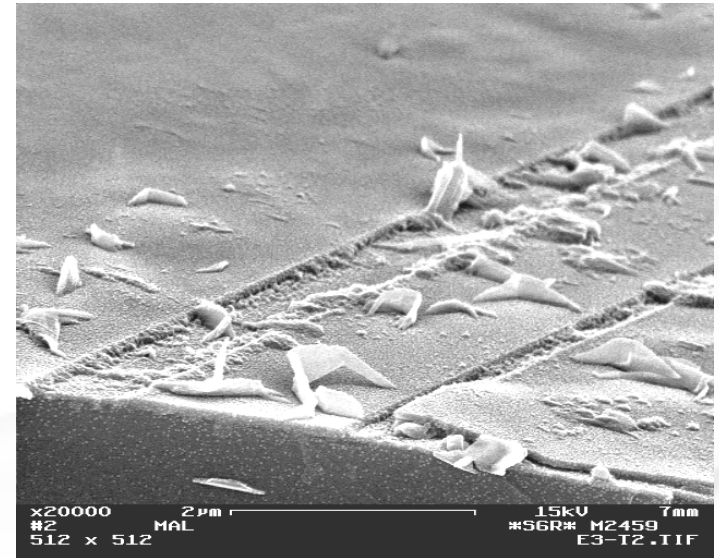
Multilayers and scratch resistance

Weak adhesion

$1 \sim 2 \text{ J/m}^2$



Scratch

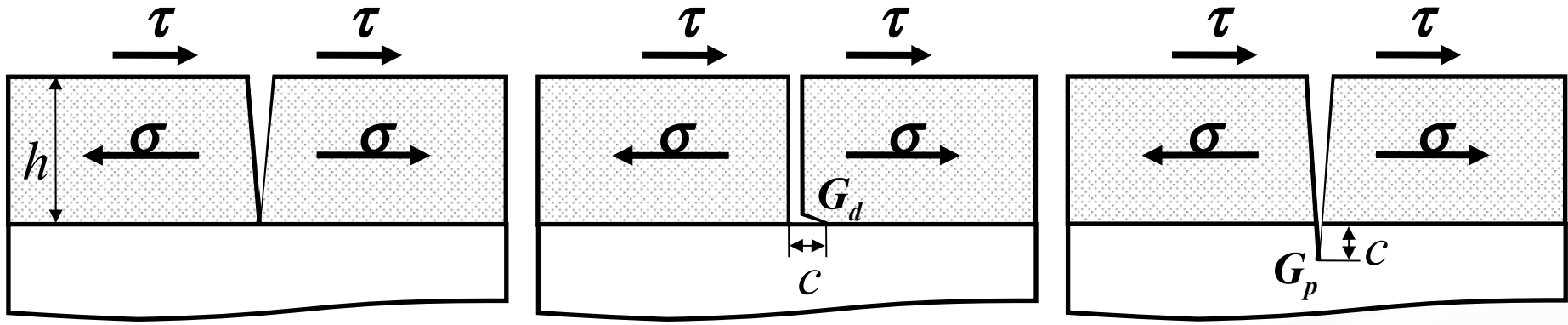


G. Duisit, S. Pelletier (TMM, SGR)

Friction

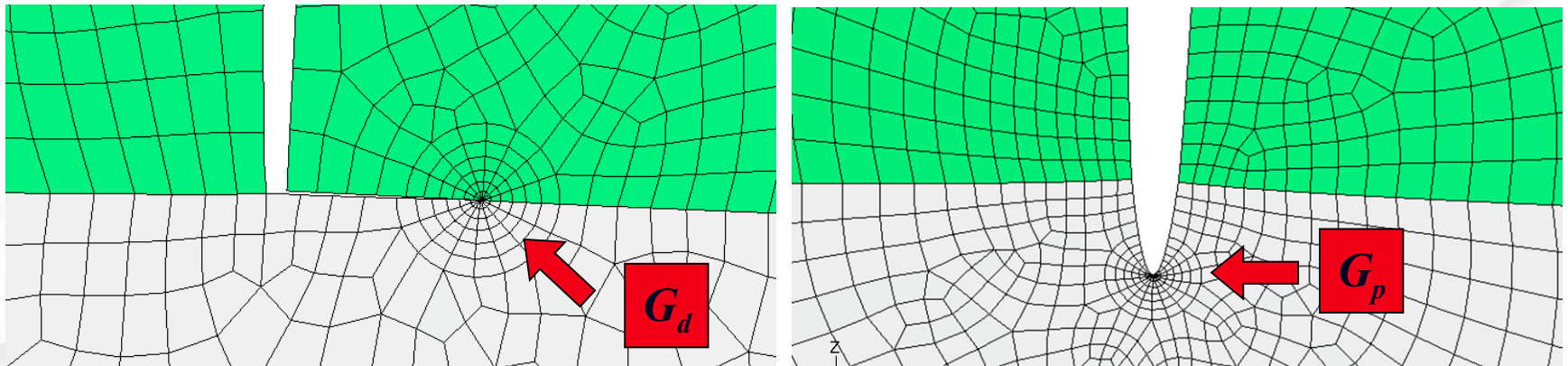
Steel/ Si_3N_4 : $\mu = 0.9$

Crack deflection



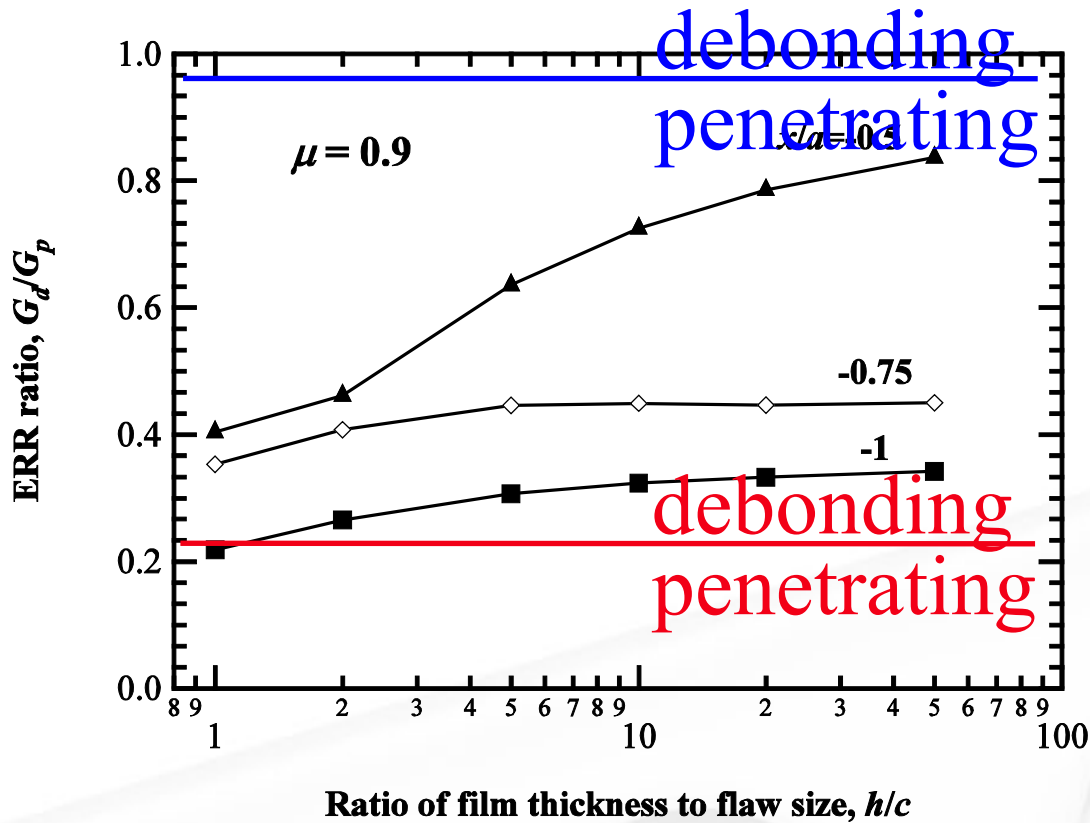
G_d : driving force for debonding along the interface

G_p : driving force for penetration into the substrate



Finite element analysis (X. Geng, Z. Zhang)

Crack deflection and adhesion



$$\Gamma_{interface} \geq 8 \text{ J/m}^2$$

Si_3N_4 monolayer



Multilayer coatings

$$\Gamma_{interface} \approx 1 \sim 2 \text{ J/m}^2$$

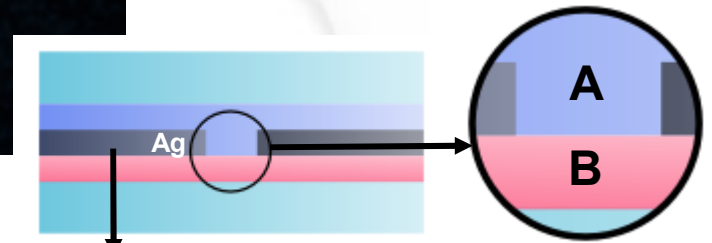
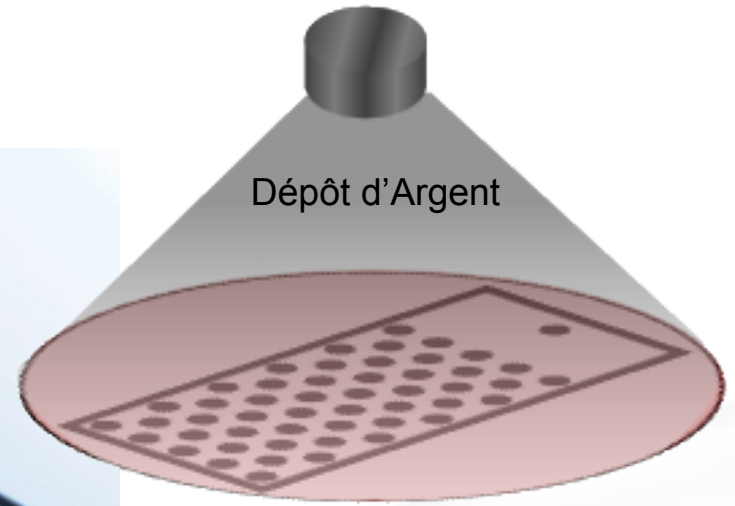
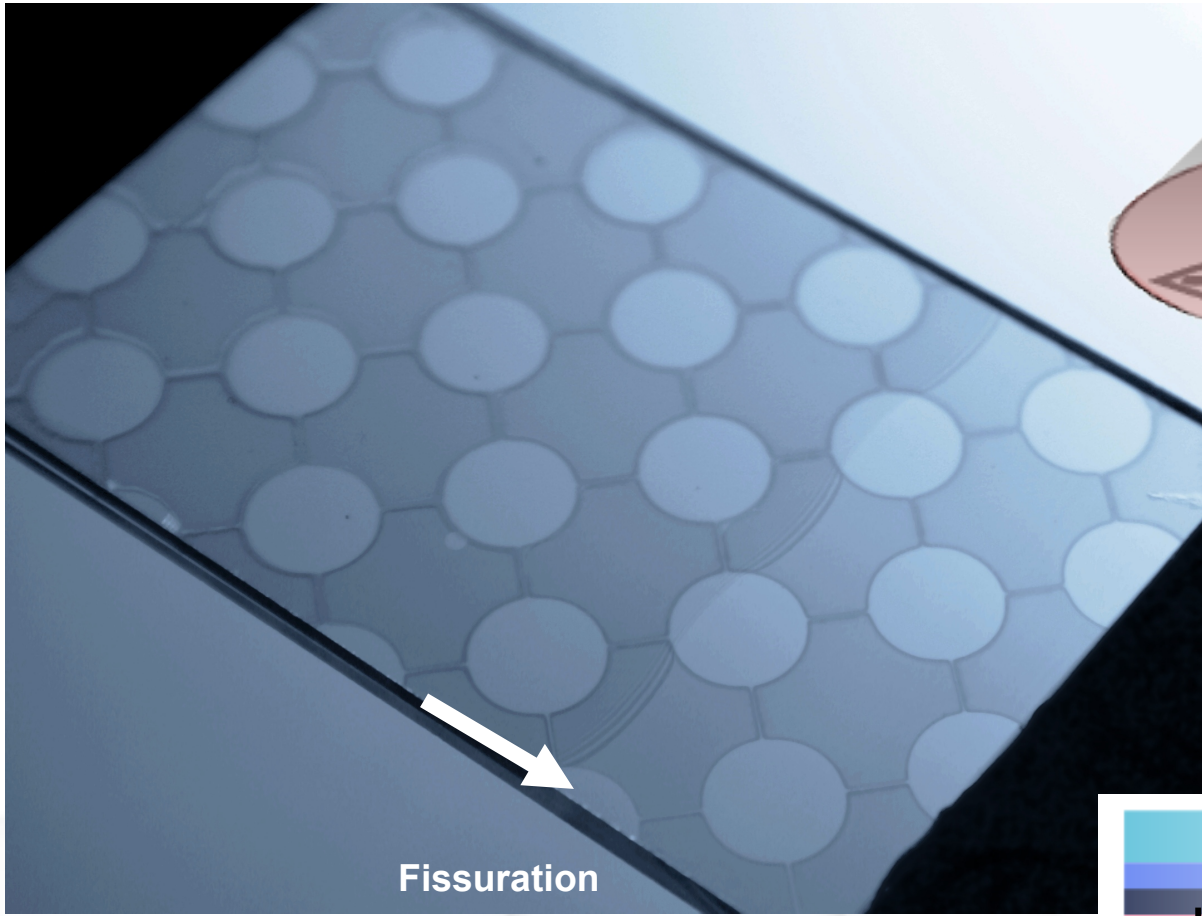
Criterion for penetrating:

$$\frac{G_d}{\Gamma_{interface}} < \frac{G_p}{\Gamma_{glass}}$$

(X. Geng, Z. Zhang)

Au delà des couches minces ?





Fissuration

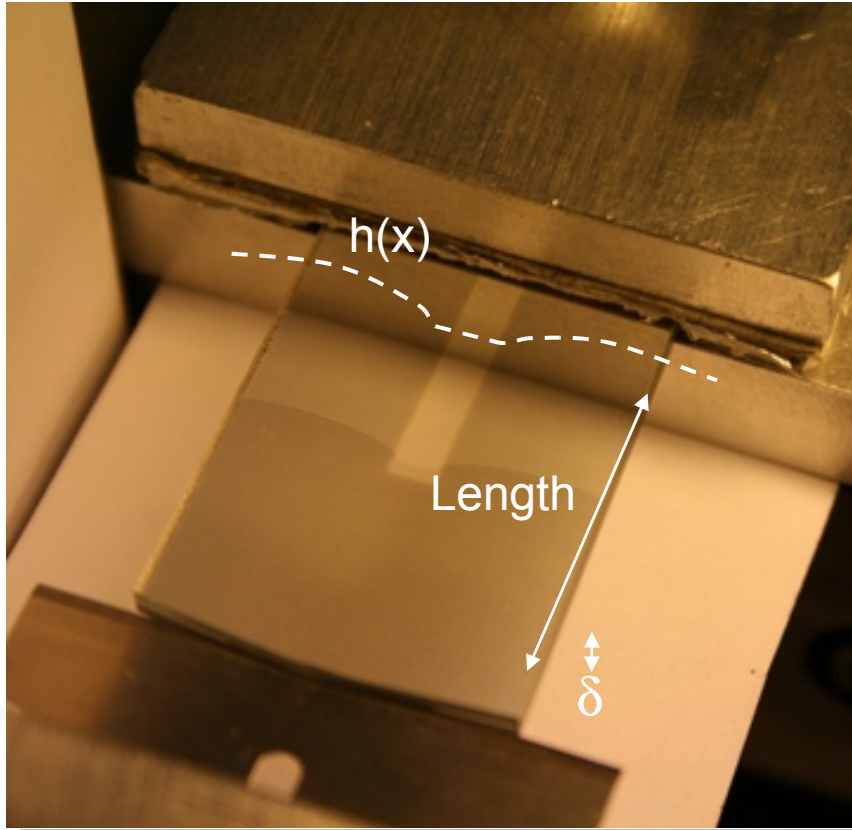
Couche d'adhésion faible

Zone d'adhésion forte

Lina Alzate



Exploitation of cleavage test



Information from cleavage test:

Global: L =Length

δ =opening

Local: Shape of the front $h(x)$

Which is the link between δ and L
and **global** adhesion?

Energy of Adhesion

$$G = - \frac{\partial U_E}{b \partial L} \propto \frac{Eh^3 \delta^2}{L^4}$$

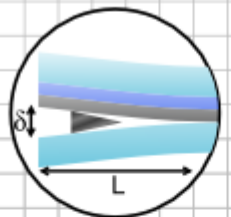
E =Young Modulus, h =Glass thickness

Lina Alzate

Effective adhesion energy of the composite interface

Global approach $G = f(\delta, L)$

Model of Kanninen

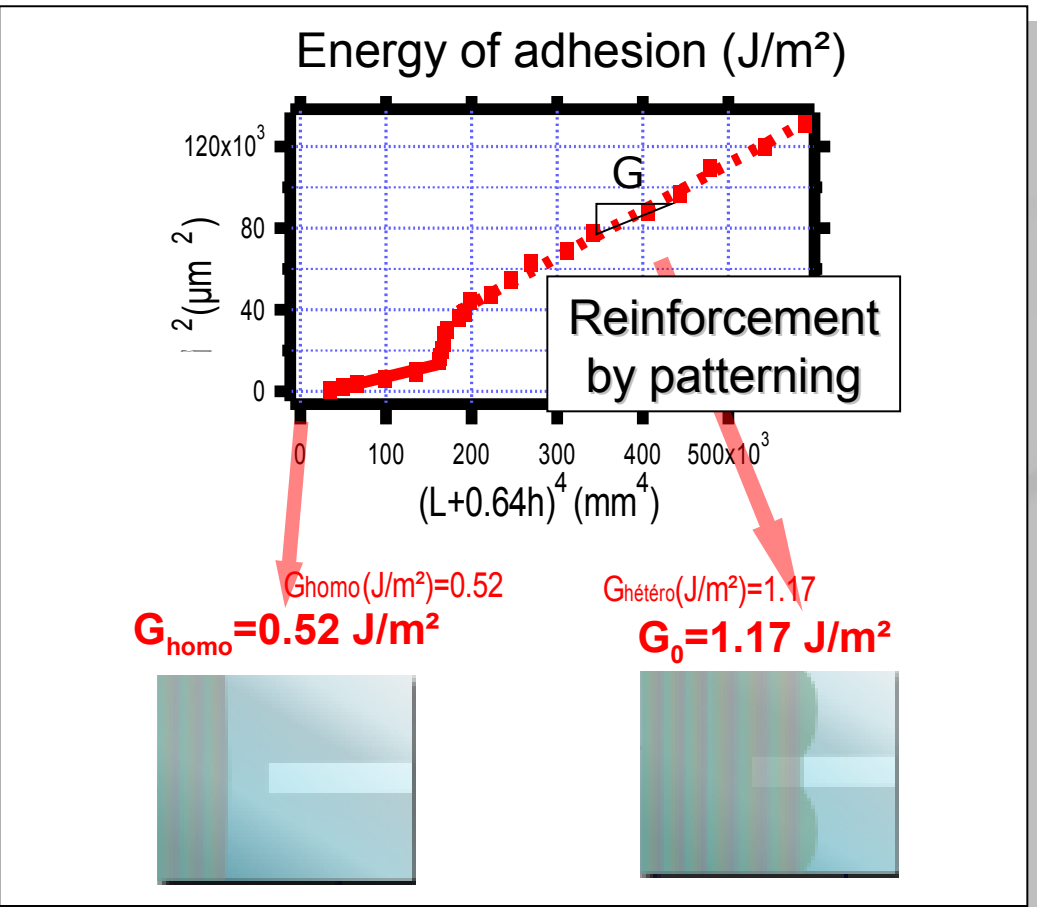


$$G = \frac{3Eh^3}{16} \frac{\delta^2}{(L + 0.64h)^4}$$

Constant

G= Energy release rate
 E= Young Modulus
 h= Glass Thickness
 delta= Crack opening
 L= Crack Length

For plane stress
 $K = \sqrt{G \cdot E}$
 K= Stress intensity factor



Can we determine the energy of adhesion of the masked zone?

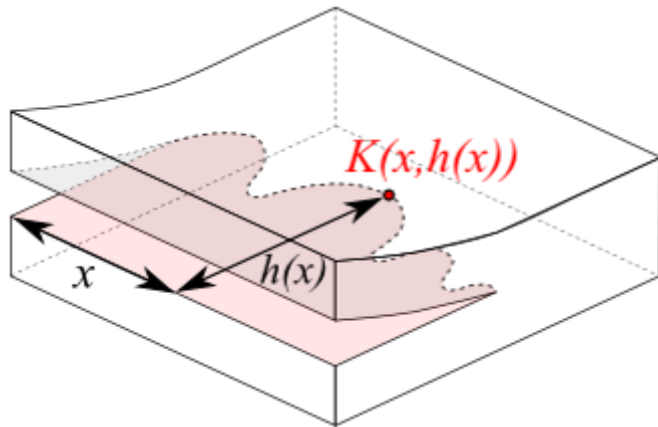
Lina Alizate

Shape of the crack front

Local approach $K = f(h(x))$

Gao et Rice, J. Appl. Mech. 56, 828 (1989)

By using a perturbative analysis, Gao and Rice propose a **local expression of K (or G) at a point $(x, h(x))$** of the front in function of the front roughness for a purely 2D crack :



Pinning Model

$$K(x, h(x)) = K_0 \left(1 + \frac{1}{2\pi} \int_{-\infty}^{+\infty} \frac{h(x) - h(x')}{(x - x')^2} dx' \right) \geq \text{Local toughness } K_C(x, h(x))$$

Where K_0 is the macroscopic toughness and $h(x)$ the in-plane front roughness

Can we validate and use this theory in an experimental way?

Validation of pinning theory

Local approach $K = f(h(x))$

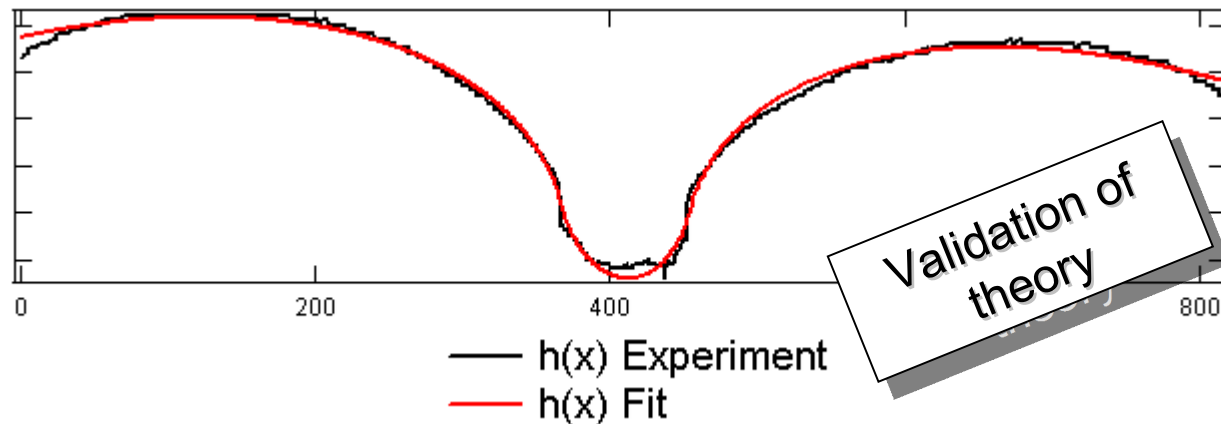
H.Gao, J.R. Rice, J. Appl. Mech 56 (1989) 828-836

Pinning Model (Gao and Rice)

$$K(x, h(x)) = K_0 \left(1 + \frac{1}{2\pi} \int_{-\inf}^{+\inf} \frac{h(x) - h(x')}{(x - x')^2} dx' \right)$$
$$h(x) = \frac{1}{\pi^2} \left(\frac{\Delta K}{K_0} \right) \{ \log(\|x\|) * a(x) \}$$

Term to fit

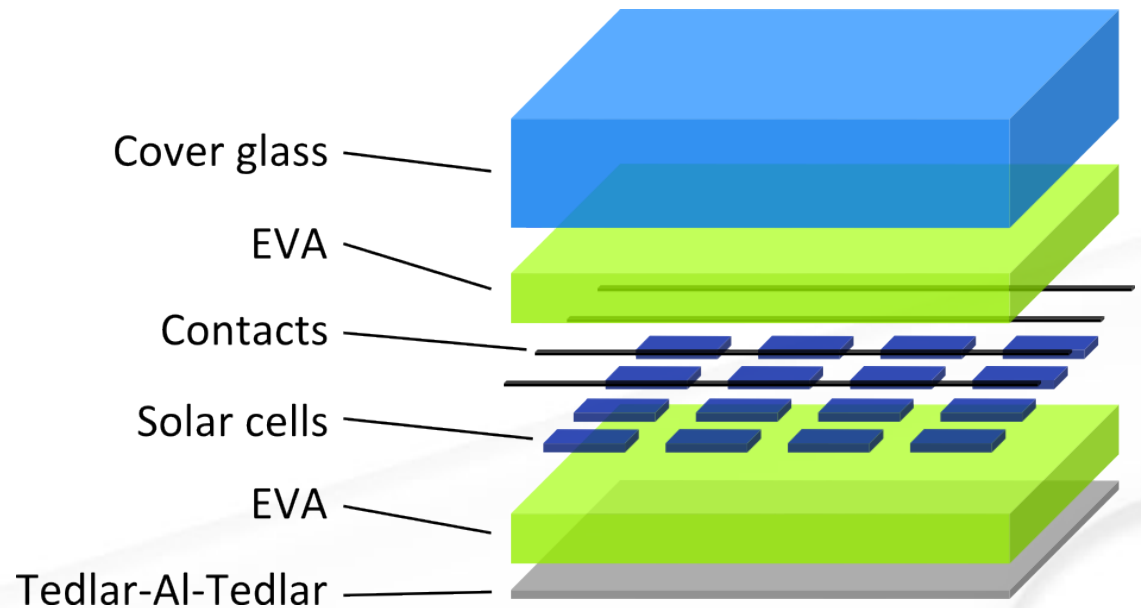
$a(x) = 0$ Outside of the masked zone
 $a(x) = 1$ Inside of the masked zone
 $h(x) =$ Crack Tip



Can we determine the value K of the masked zone ?

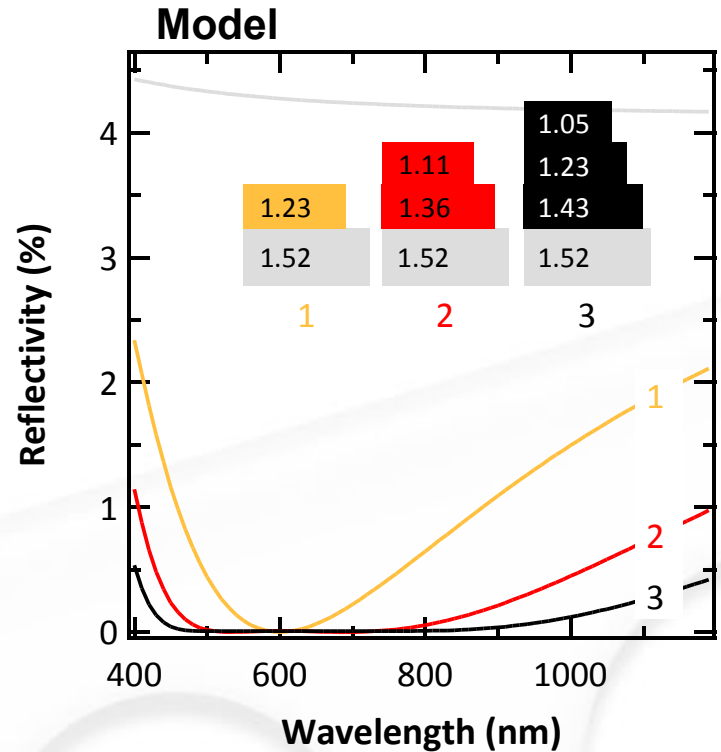
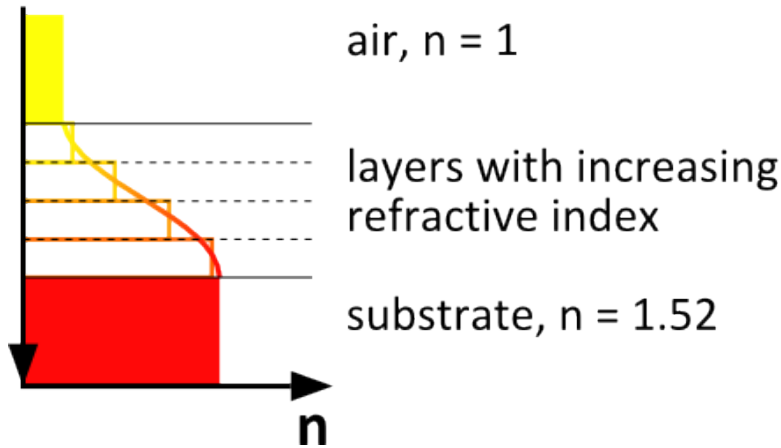
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Solar cells encapsulation



**~4% reflection of solar light
on glass surface**

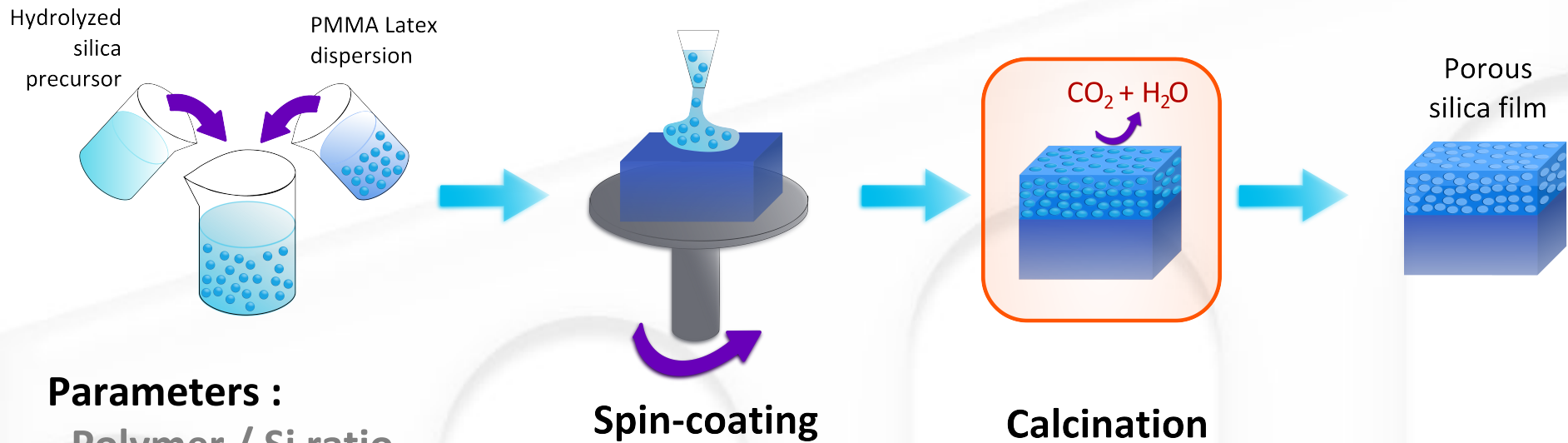
Index-gradient anti-reflective coatings



- Low angular variation
- Wide band
- Need for very low refractive index

Latex templated silica films

- Organic nanoparticles as sacrificial template

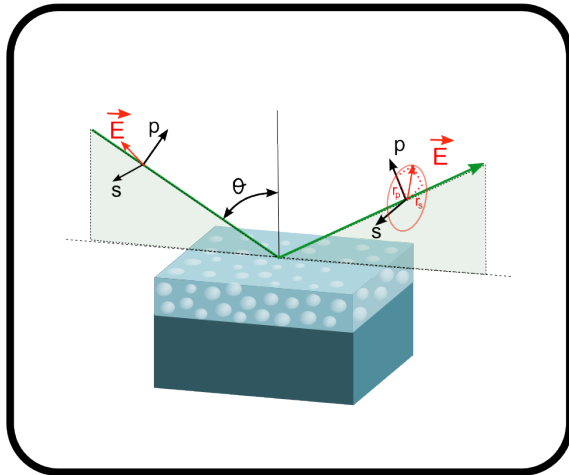


Parameters :

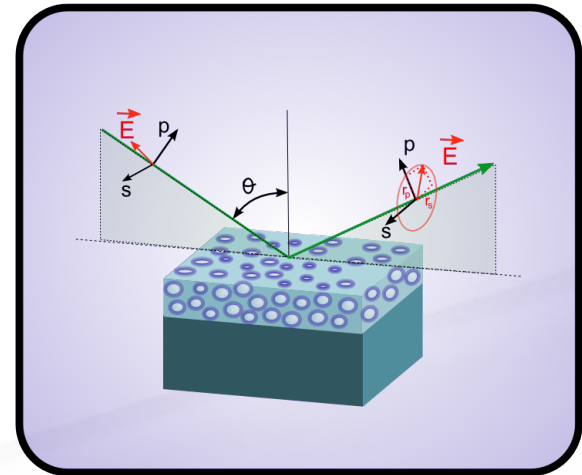
- Polymer / Si ratio
- Nanoparticles size
- Dilution

Pore structure : ellipsometry-porosimetry

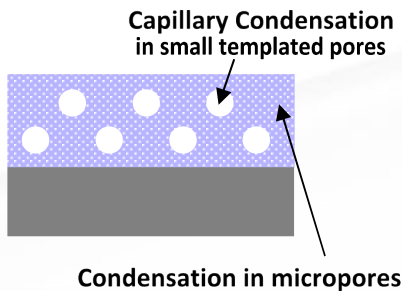
Vacuum vessel



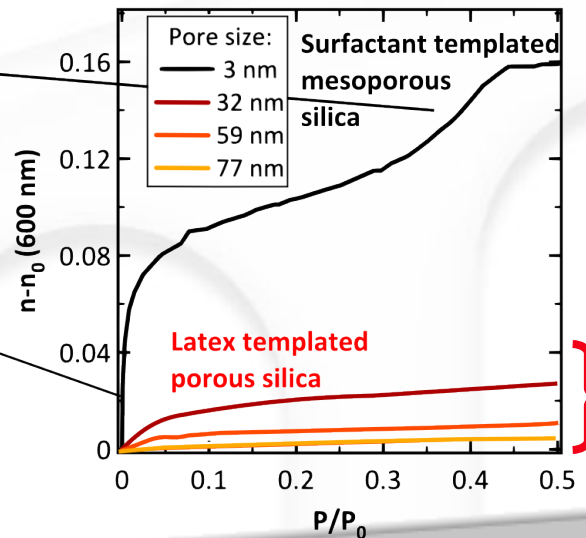
Progressive introduction
of an adsorbant



Surfactant template



Adsorption isotherm



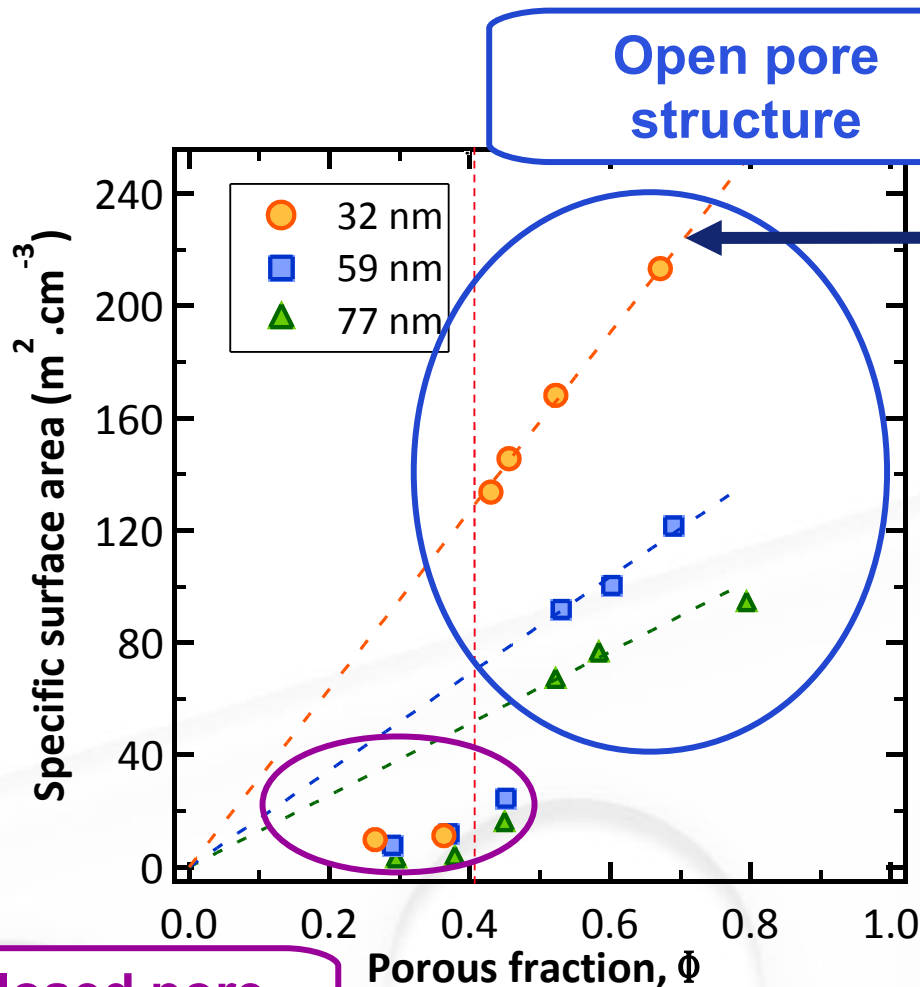
Latex template



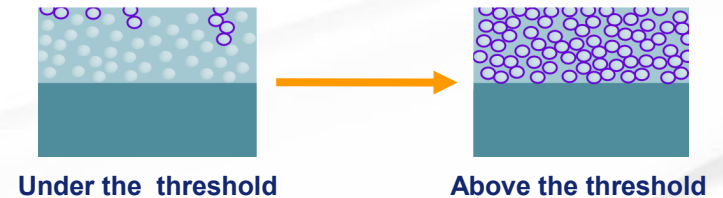
Pore size >30 nm :
Stable refractive index

François Guillemot

Pore structure : specific surface area



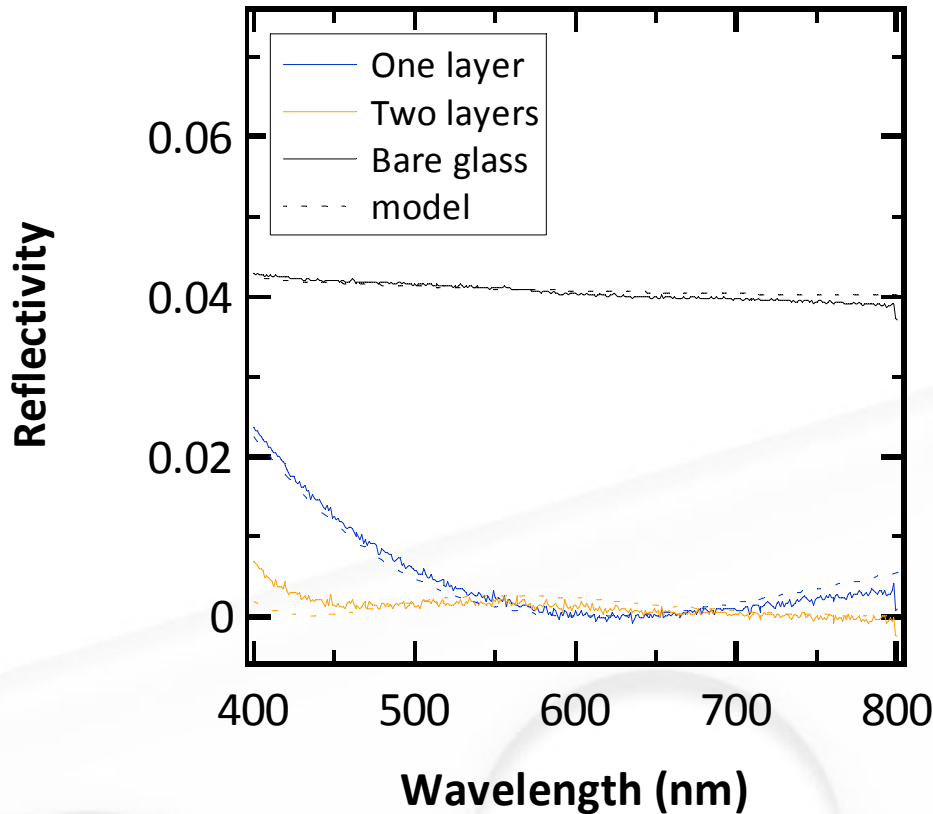
Geometry : $S_{spe} \propto \frac{\Phi}{d_{pore}}$



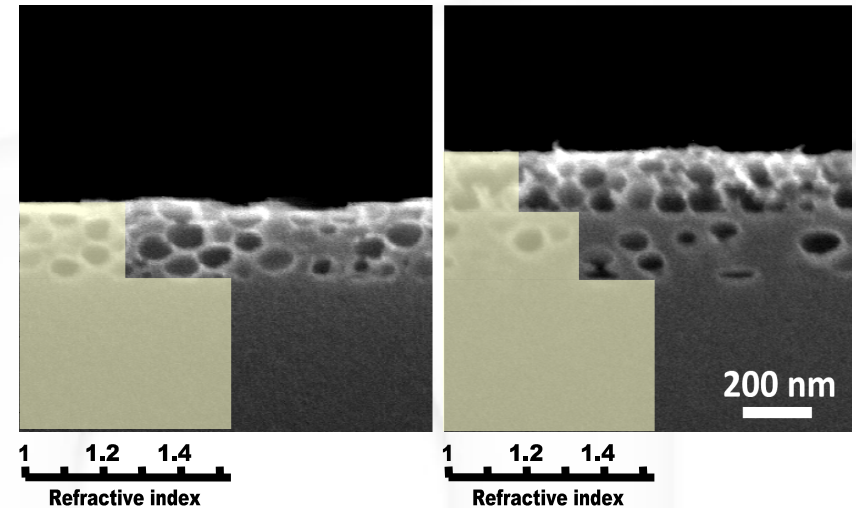
Percolation transition

- Scale invariance
- Threshold around 40%

Index gradient antireflective stacks

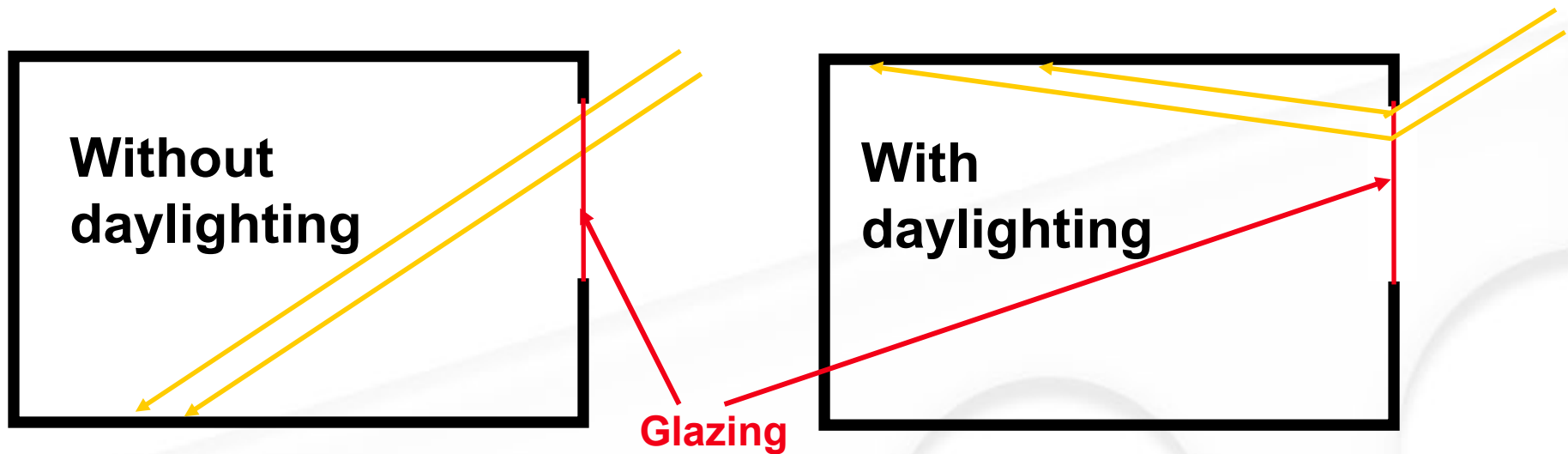


Flatter reflectivity with smoother refractive index gradient



Modeling with CAMFR : *Peter Bienstman, PhD Thesis, Ghent University, Belgium, 2001* (<http://camfr.sourceforge.net>)

Daylighting – Principle



Daylighting – Application

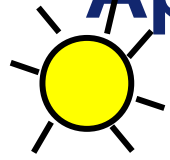


SGG Lumitop®

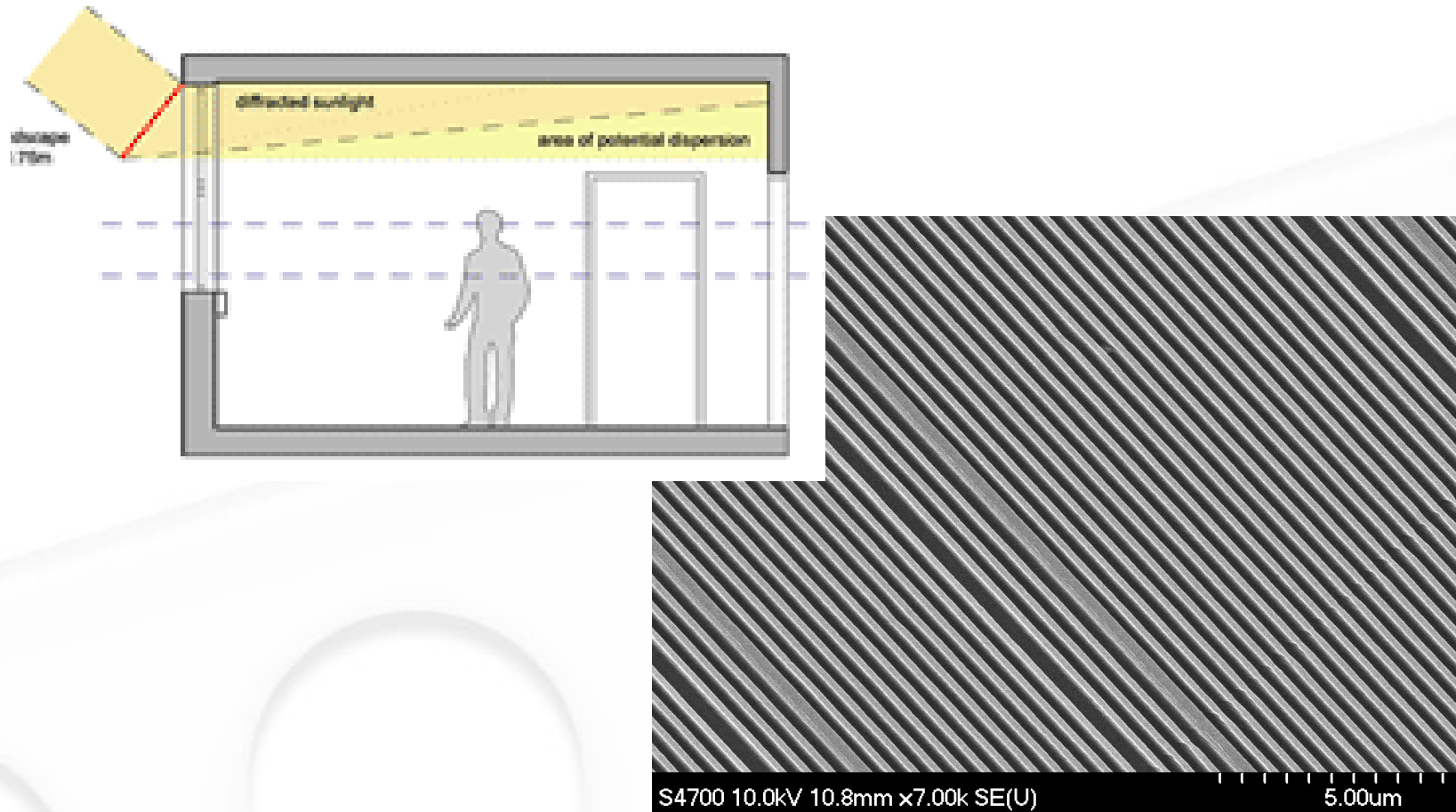
**Eckelt
Ecklite®**

**Redbus
Serraglaze®**

Applications : miscellenaous



Daylighting glazing



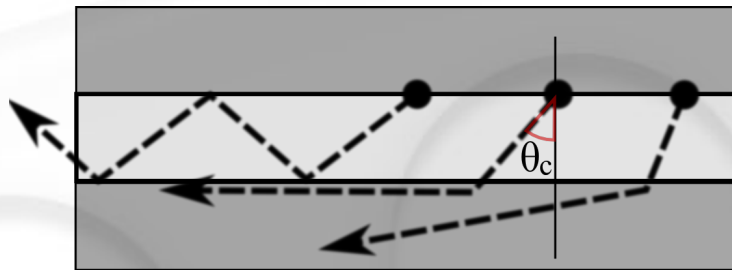
Saint-Gobain Recherche / O2M



Application : LEDs



die	λ (nm)	n_{die}	n_{encaps}	θ_c	$1 - \cos \theta_c$
alumina	589	1.76	1.0	34	0.18
alumina	589	1.76	1.5	60	0.49
GaN	411	2.5	1.0	24	0.08
GaN	411	2.5	1.5	37	0.2
GaAs	589	4.02	1.0	14	0.03
GaAs	589	4.02	1.5	22	0.07



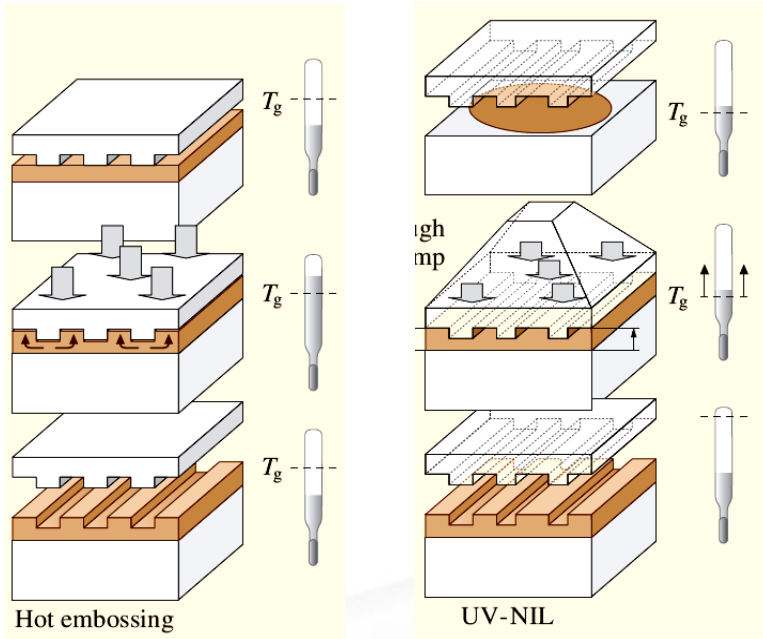
$$\sin \theta_c = \frac{n_{encap}}{n_{die}}$$

$$X_{tot} = 1 - \cos \theta_c$$

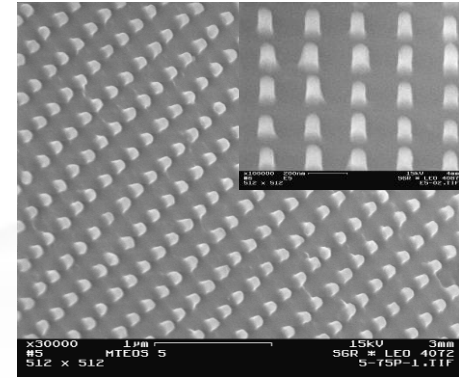
Contexte

C. Peroz et al., *J Vac Sci Tech B*, **2007**, 25(4) L27
 C. Peroz et al., *Advanced Material*, **2009**, 21(5) 555
 PCT/FR2008/050594 C.Peroz, E. Sondergard E. Barthel

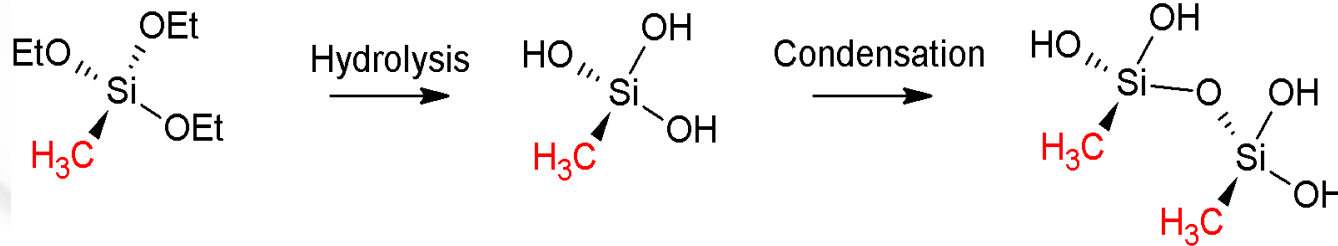
Procédé d'impression



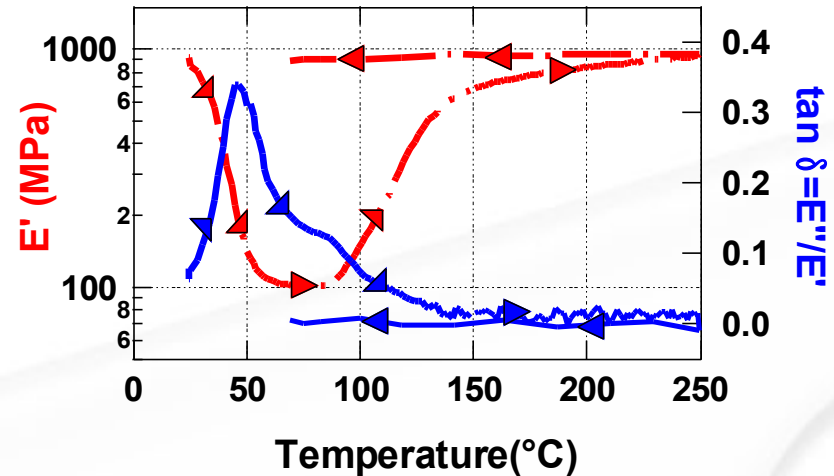
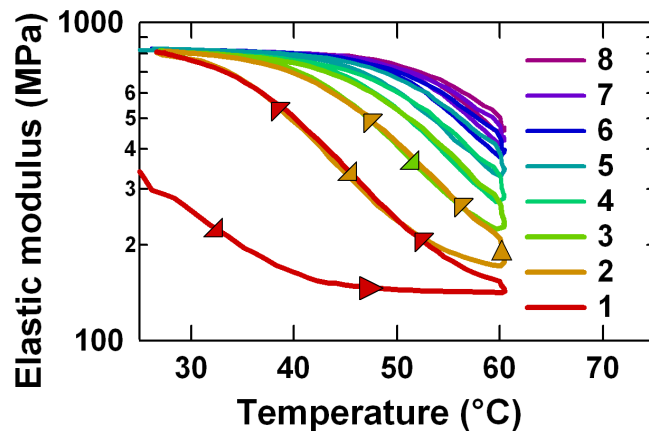
Obtention de structures avec une faible période et des rapports d'aspects >1



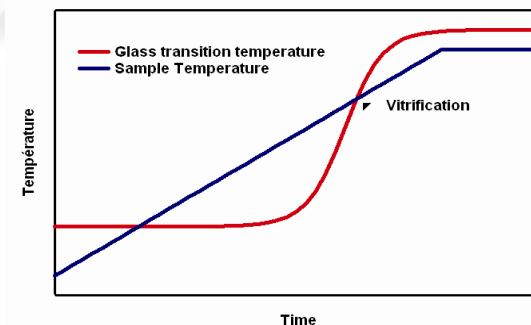
dots ($\varnothing=75\text{nm}$, $p=230\text{nm}$, $h=150\text{nm}$)



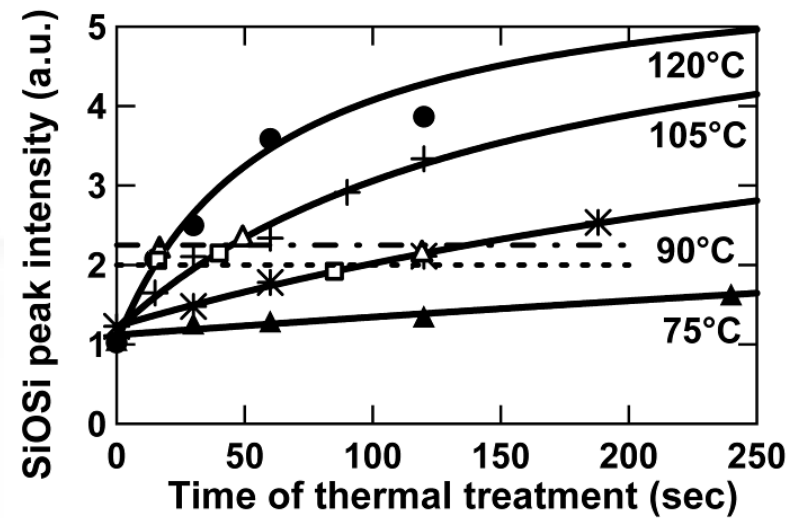
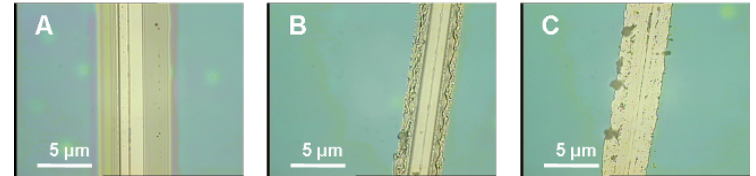
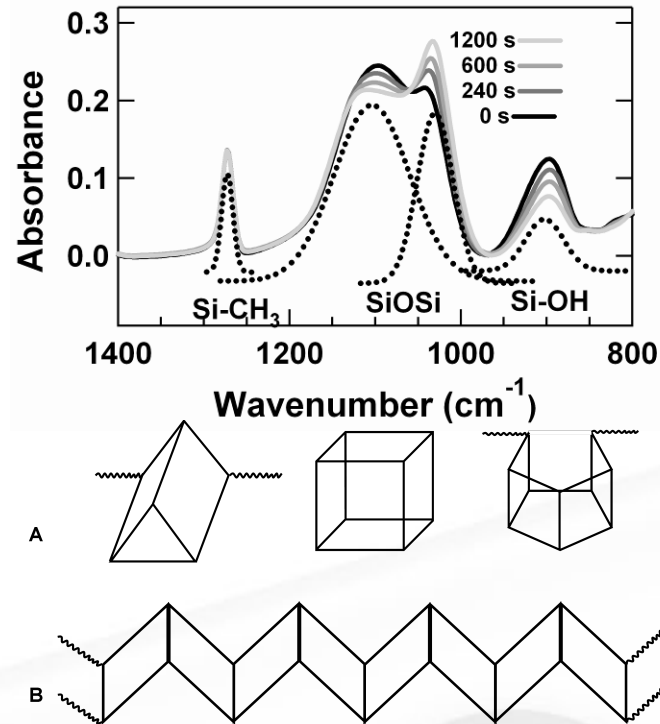
DMA: mise en évidence d'une T_g et évolution durant le traitement thermique



- T_g initial proche de 30°C
- Augmentation progressive de la T_g avec la condensation
- La vitrification a lieu quand $T_g = T_{\text{échantillon}}$

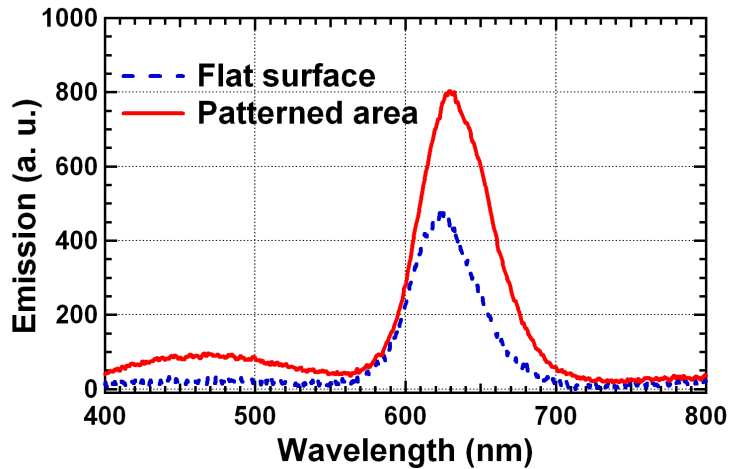
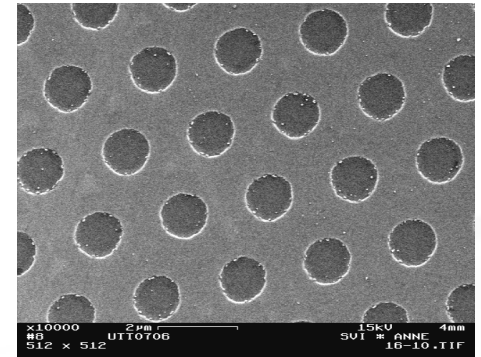
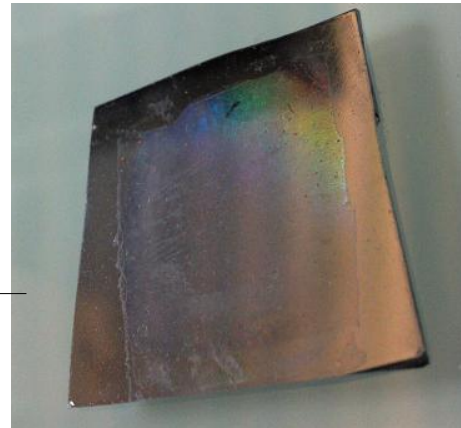
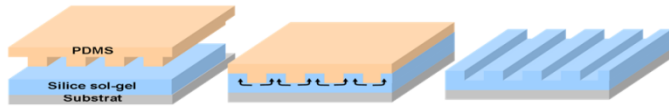


Rappel: Etude structure interne



- 2 modes de vibrations SiOSi
- Un seuil de condensation indépendant de la température pour la vitrification

Etude de l'influence de la structuration



Luminescence observée sur les films
Augmentation de la luminescence pour les
zones structurées

- comprendre la physique de la surface texturée
- développer les moyens d'élaboration pour les surfaces de grande taille